



Optimising Test Mass Position for the LISA- Pathfinder Optical Metrology System

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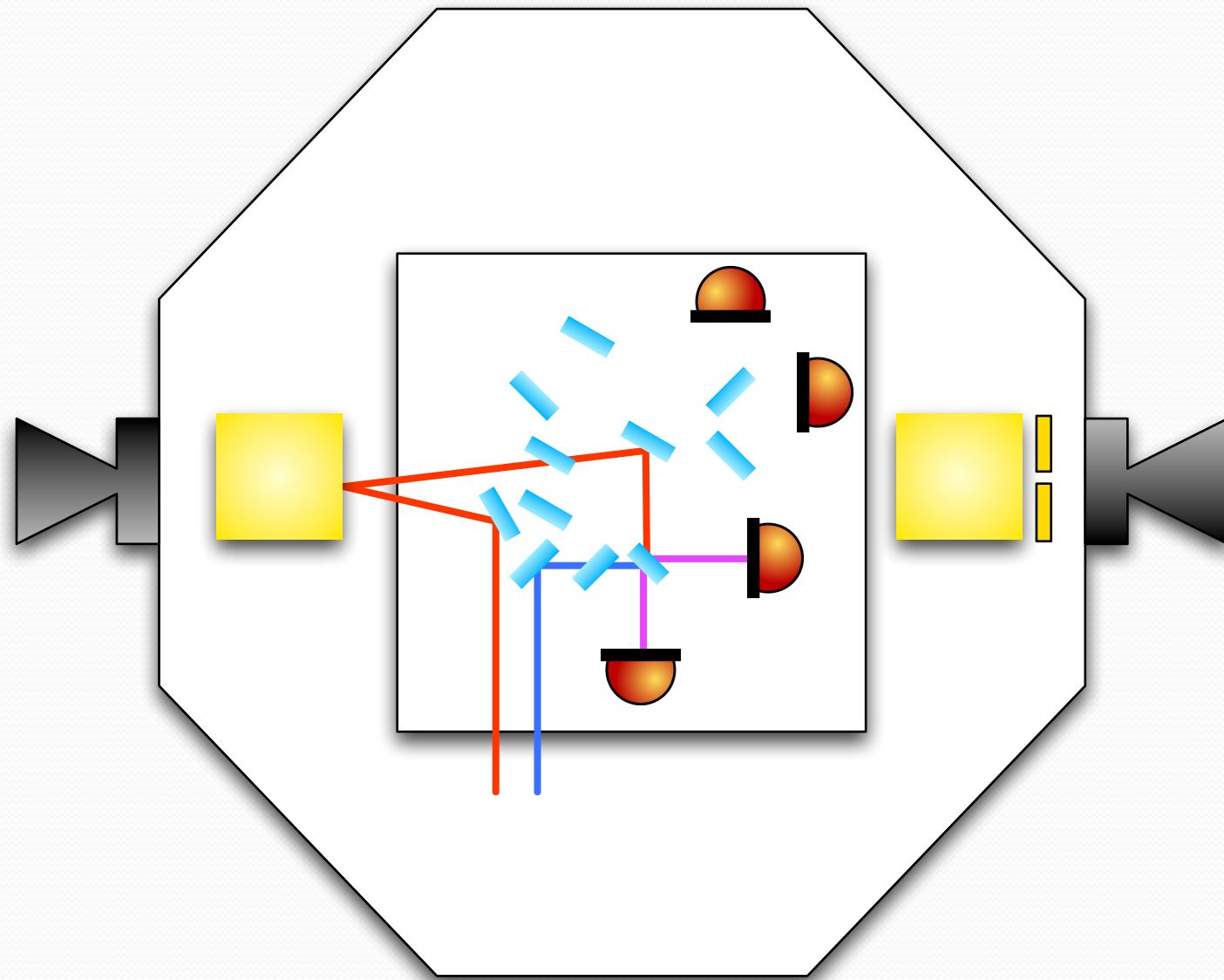


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Germany

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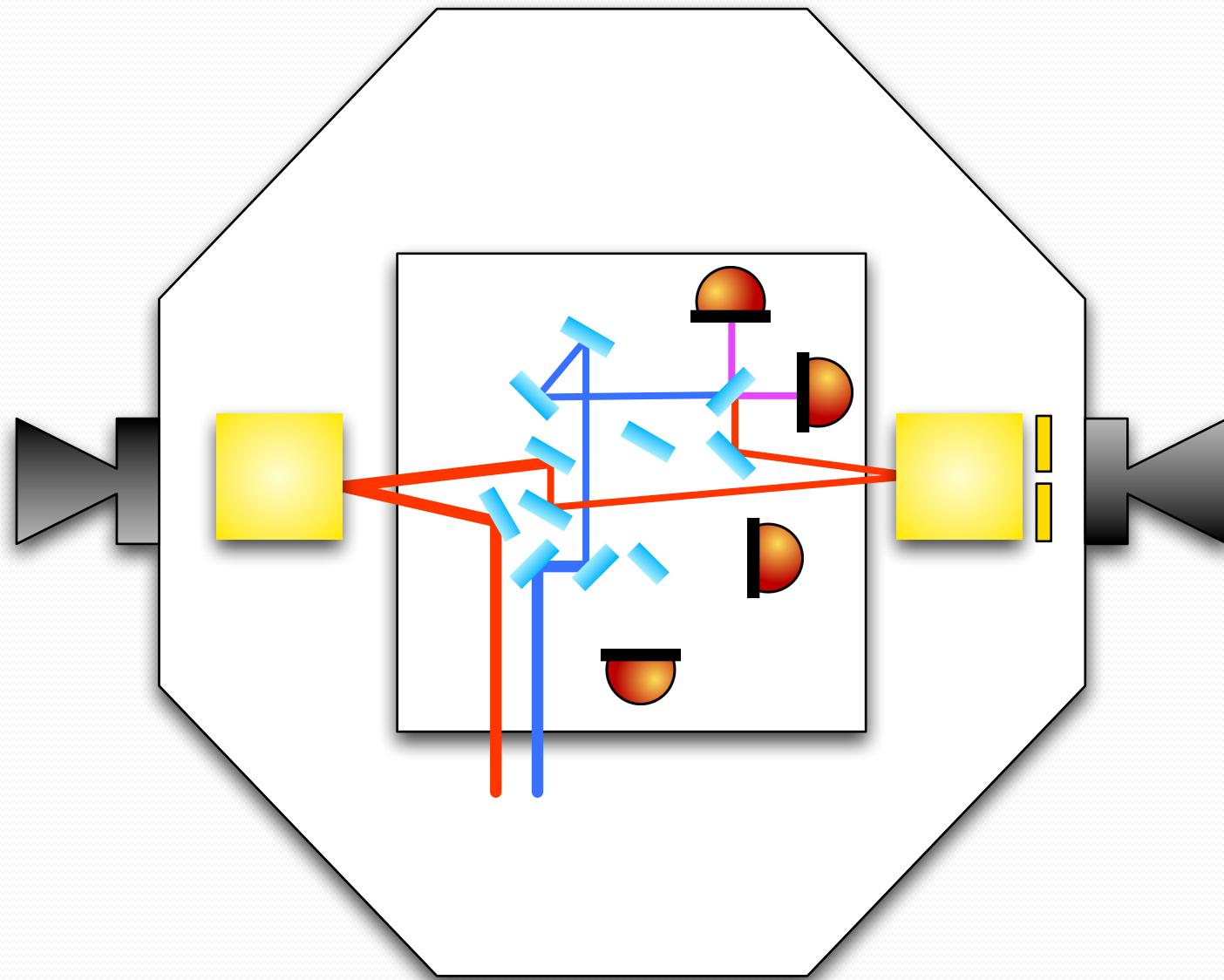


LPF x-Axis Measurement





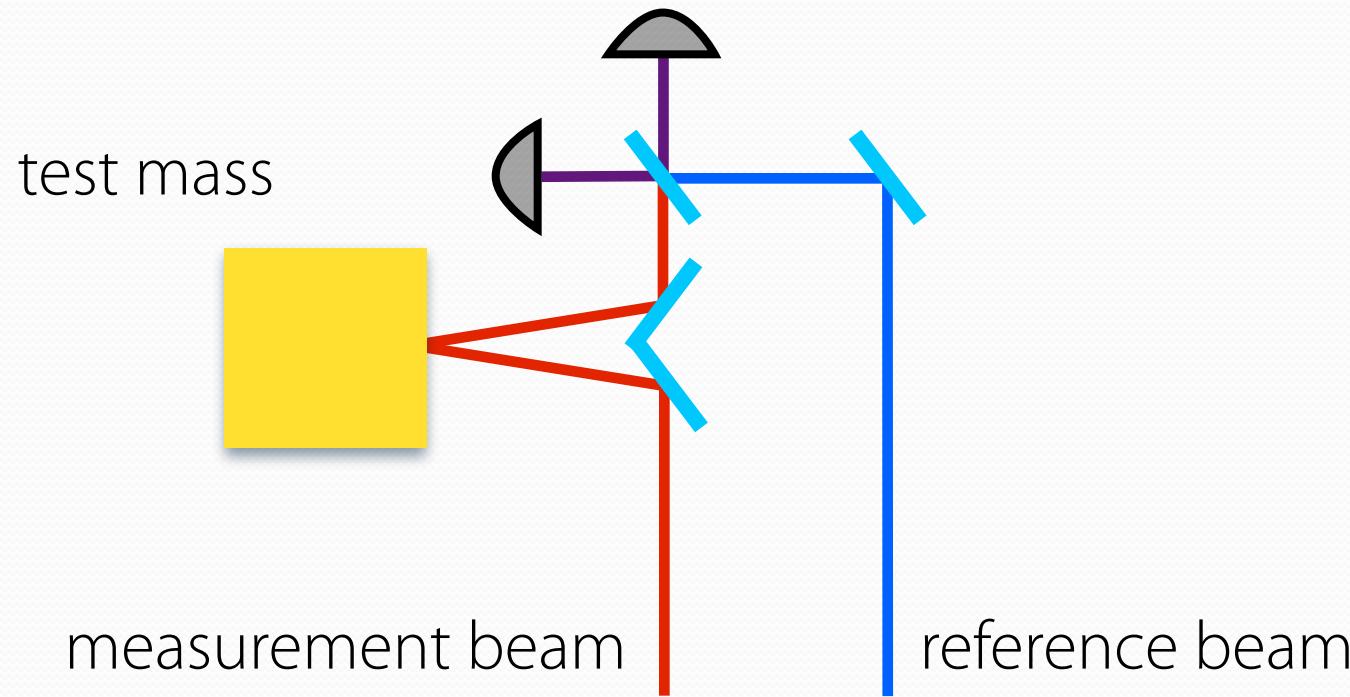
LPF x-Axis Measurement





Interferometry

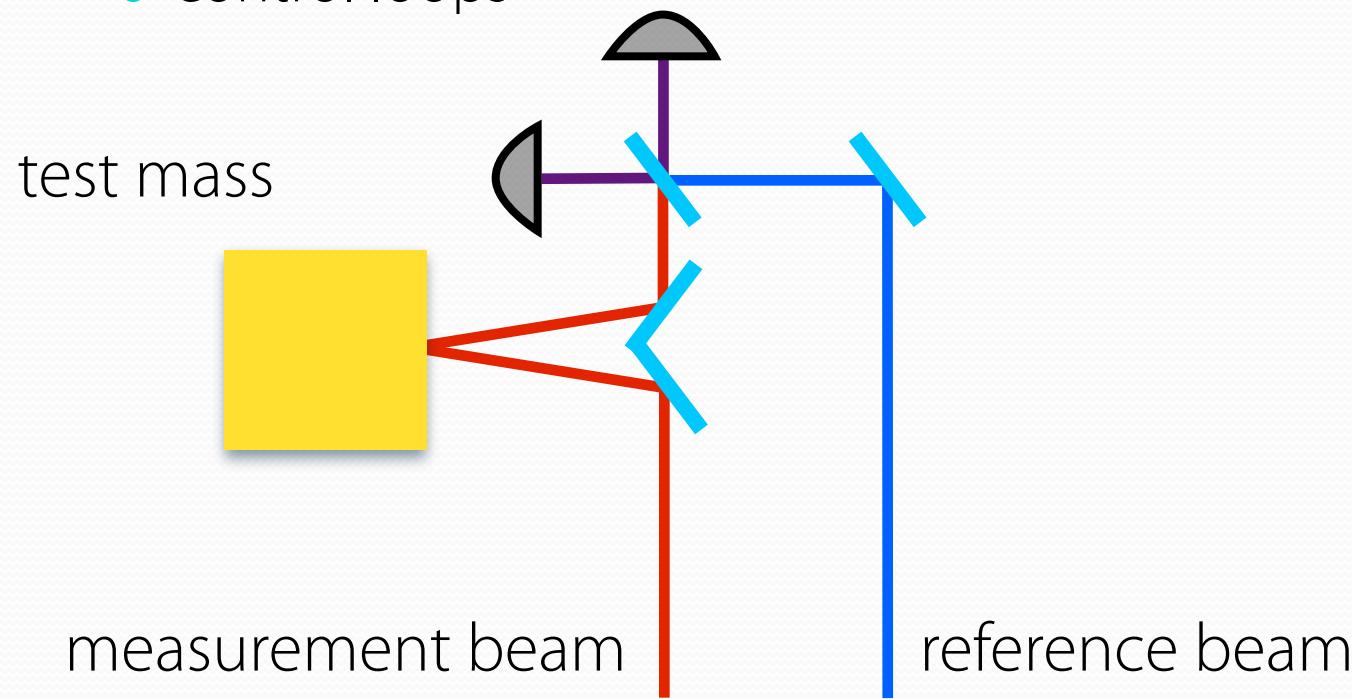
- interferometer signal
 - optical path length difference noise
 - amplitude noise
 - frequency noise





Interferometry

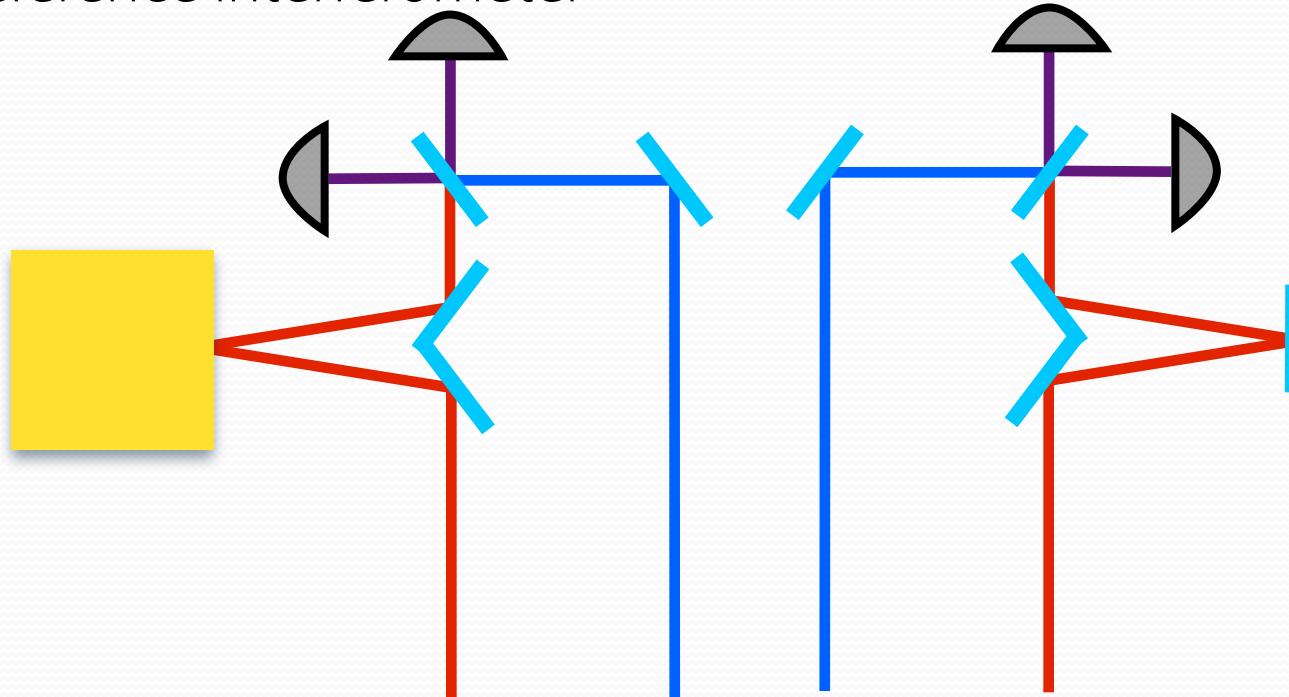
- interferometer signal
 - optical path length difference noise
 - amplitude noise
 - frequency noise
- control loops





Interferometry

- interferometer signal
 - optical path length difference noise
 - amplitude noise
 - frequency noise
- reference interferometer





Reference signal subtraction

Common mode noise rejection properties of amplitude and phase noise in a heterodyne interferometer

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High precision metrology systems based on heterodyne interferometry can measure position and attitude of objects to accuracies of picometer and nanorad, respectively. A frequently found feature of the general system design is the subtraction of a reference phase from the phase of the position interferometer, which suppresses low frequency common mode amplitude and phase fluctuations occurring in volatile optical path sections shared by both, the position and reference interferometer. Spectral components of the noise at frequencies higher than the heterodyne frequency, however, are generally transmitted into the measurement band and may limit the measurement accuracy. Detailed analytical calculations complemented with Monte Carlo simulations show that high frequency noise components may also be entirely suppressed, depending on the relative difference of measurement and reference phase, which may be exploited by corresponding design provisions. Whilst these results are applicable to any heterodyne interferometer with certain design characteristics, specific calculations and related discussions are given for the example of the optical metrology system of the LISA Pathfinder mission to space.

OCIS codes: 120.3940, 120.3180, 040.2840, 100.5070



Interferometer signals



- Flight model uses both photodiodes
 - subtraction of common mode amplitude noise

$$F_{i,j} = \begin{cases} \frac{1}{2}(F_{i,j,A} + F_{i,j,B}) & \text{A and B OK} \\ F_{i,j,A} & \text{A OK, B failure} \\ F_{i,j,B} & \text{B OK, A failure} \\ \text{Non - computable} & \text{A and B failure} \end{cases}$$



Interferometer signals

- Flight model uses both photodiodes
 - one photodiode could fail
 - beamsplitter not 50/50
 - measure limiting noise source



Amplitude noise

$$\phi_n - \psi_n$$

$$\Delta n_{\text{an}} = \Delta\phi_{\text{an}} - \Delta\psi_{\text{an}}$$

measurement signal

reference signal

remaining amplitude noise



Amplitude noise

$$\phi_n - \psi_n$$

$$\Delta n_{\text{an}} = \Delta\phi_{\text{an}} - \Delta\psi_{\text{an}}$$

$$\langle \Delta n_{\text{an}}^2 \rangle = \frac{2}{NA_{\text{in}}^2} \langle n_k^2 \rangle 4 \sin^2 (\psi/2)$$

remaining amplitude noise

injected amplitude noise

phase difference

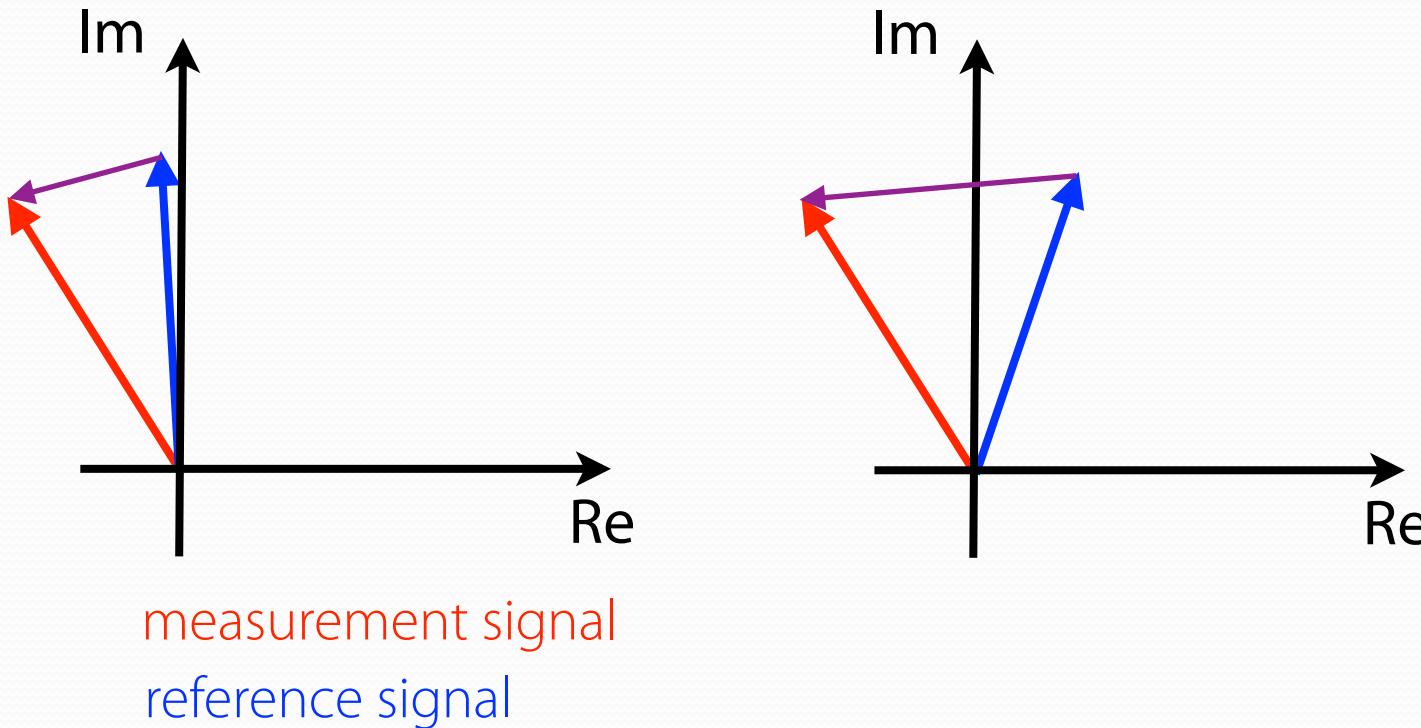


Amplitude noise

$$\phi_n - \psi_n$$

$$\Delta n_{\text{an}} = \Delta\phi_{\text{an}} - \Delta\psi_{\text{an}}$$

$$\langle \Delta n_{\text{an}}^2 \rangle = \frac{2}{NA_{\text{in}}^2} \langle n_k^2 \rangle 4 \sin^2 (\psi/2)$$



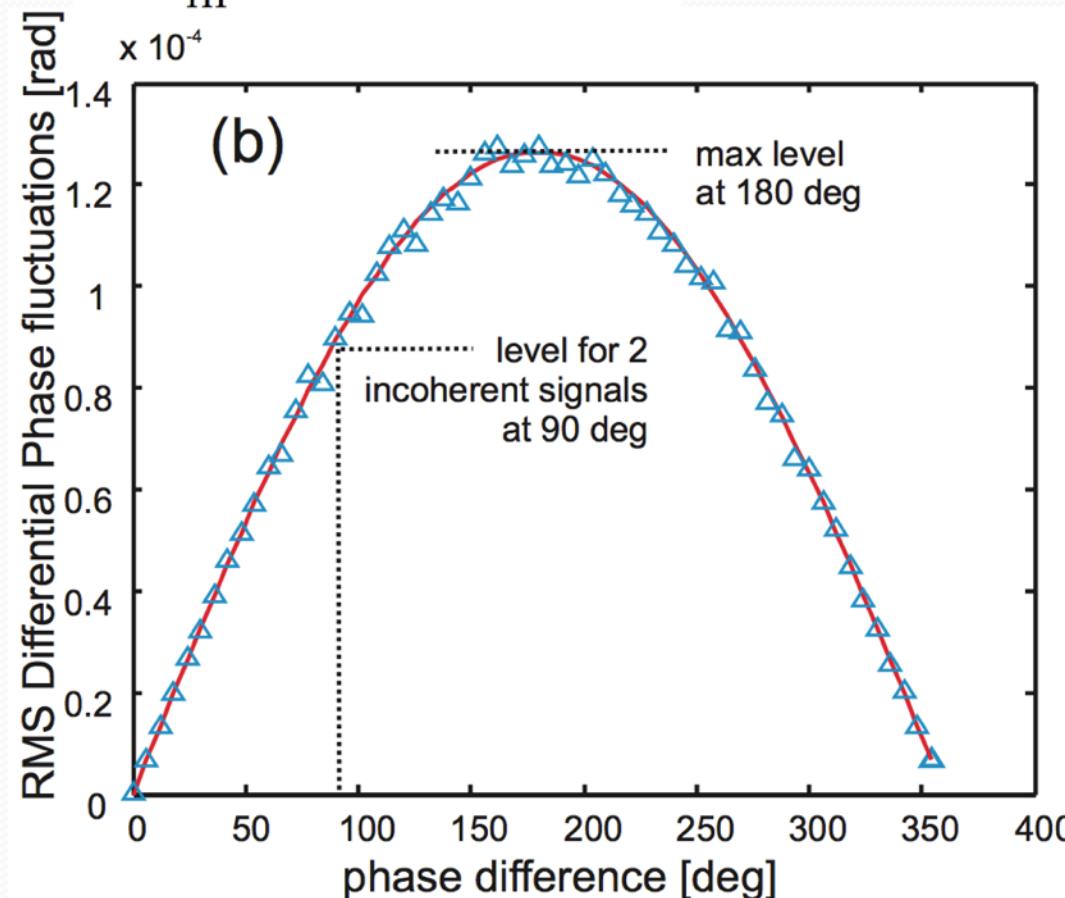


Amplitude noise

$$\phi_n - \psi_n$$

$$\Delta n_{\text{an}} = \Delta\phi_{\text{an}} - \Delta\psi_{\text{an}}$$

$$\langle \Delta n_{\text{an}}^2 \rangle = \frac{2}{NA_{\text{in}}^2} \langle n_k^2 \rangle 4 \sin^2 (\psi/2)$$



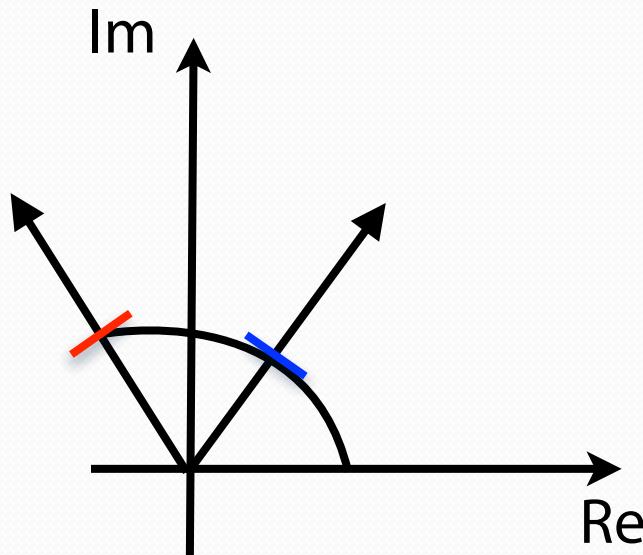


OPD noise

$$\phi_n - \psi_n$$

$$\Delta n_{\text{pn}} = (\phi_{\text{pn}} - \psi_{\text{pn}}) - (\phi - \psi)$$

$$= \frac{2}{N} \langle n_k^2 \rangle \sin^2(\phi - \psi)$$





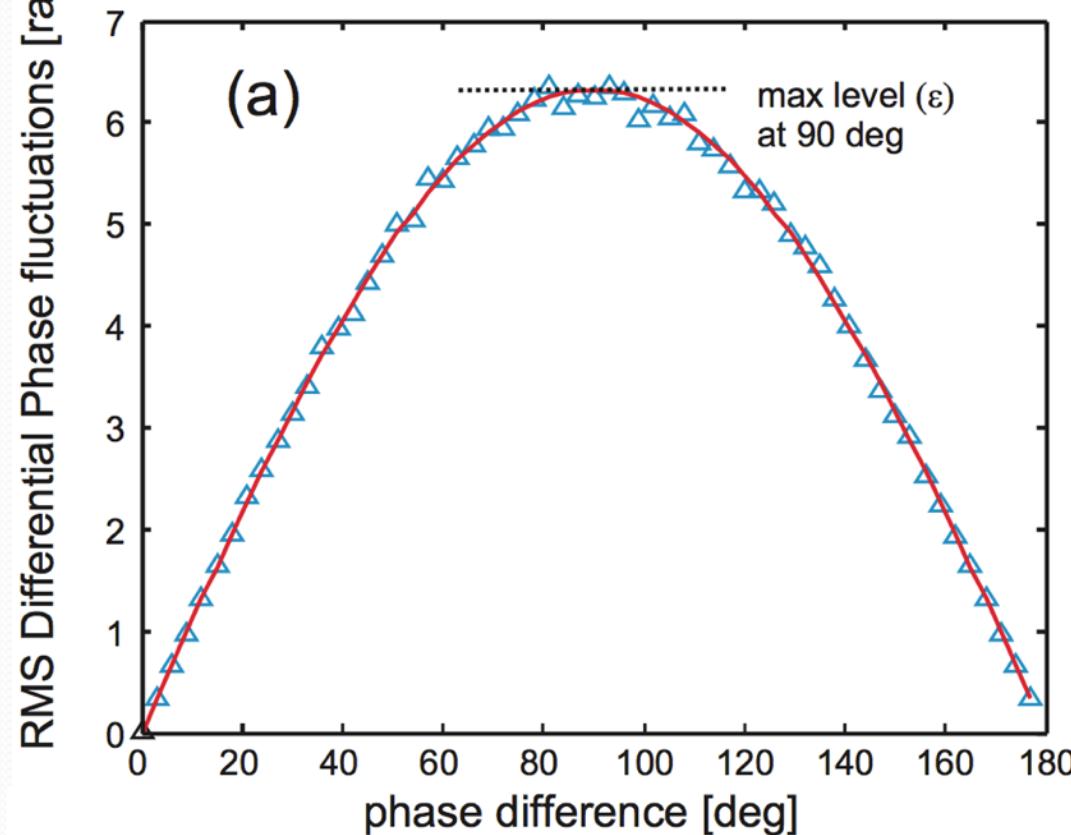
OPD noise

$$\phi_n - \psi_n$$

$$\Delta n_{pn} = (\phi_{pn} - \psi_{pn}) - (\phi - \psi)$$

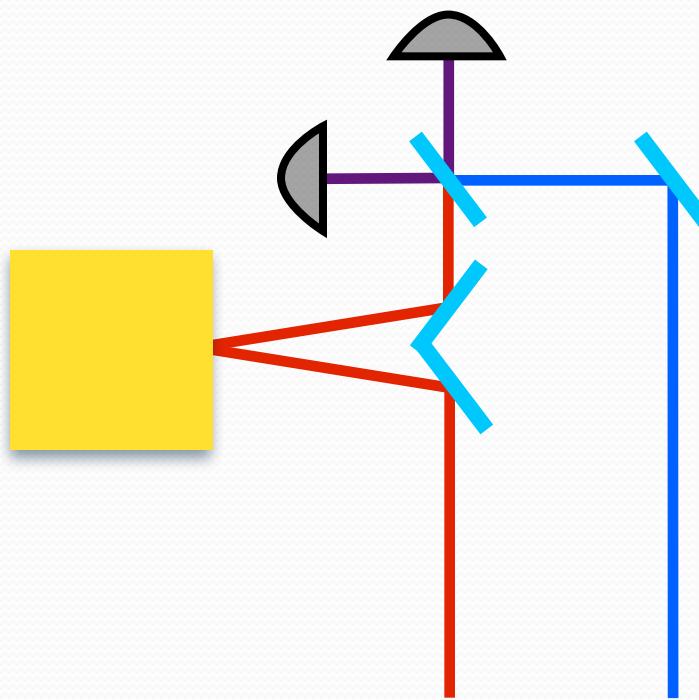
$$= \frac{2}{N} \langle n_k^2 \rangle \sin^2(\phi - \psi)$$

$\times 10^{-5}$

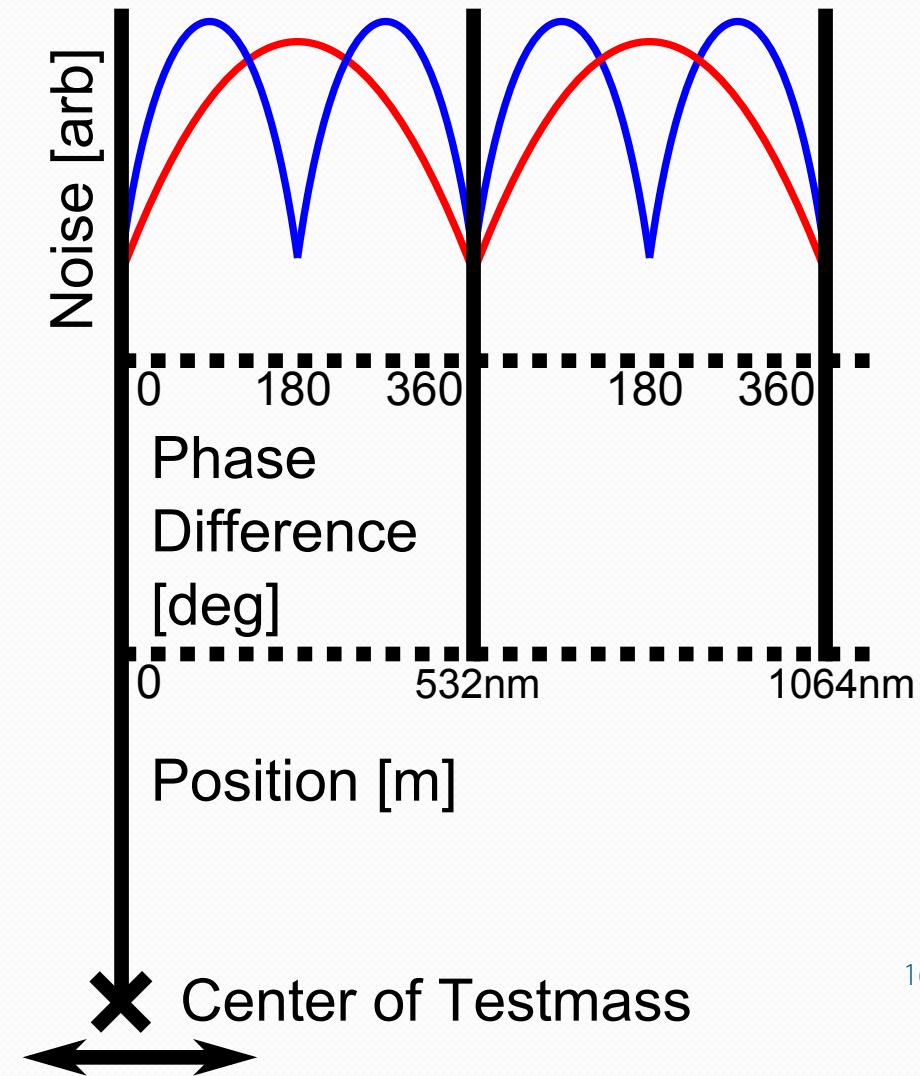




Summary

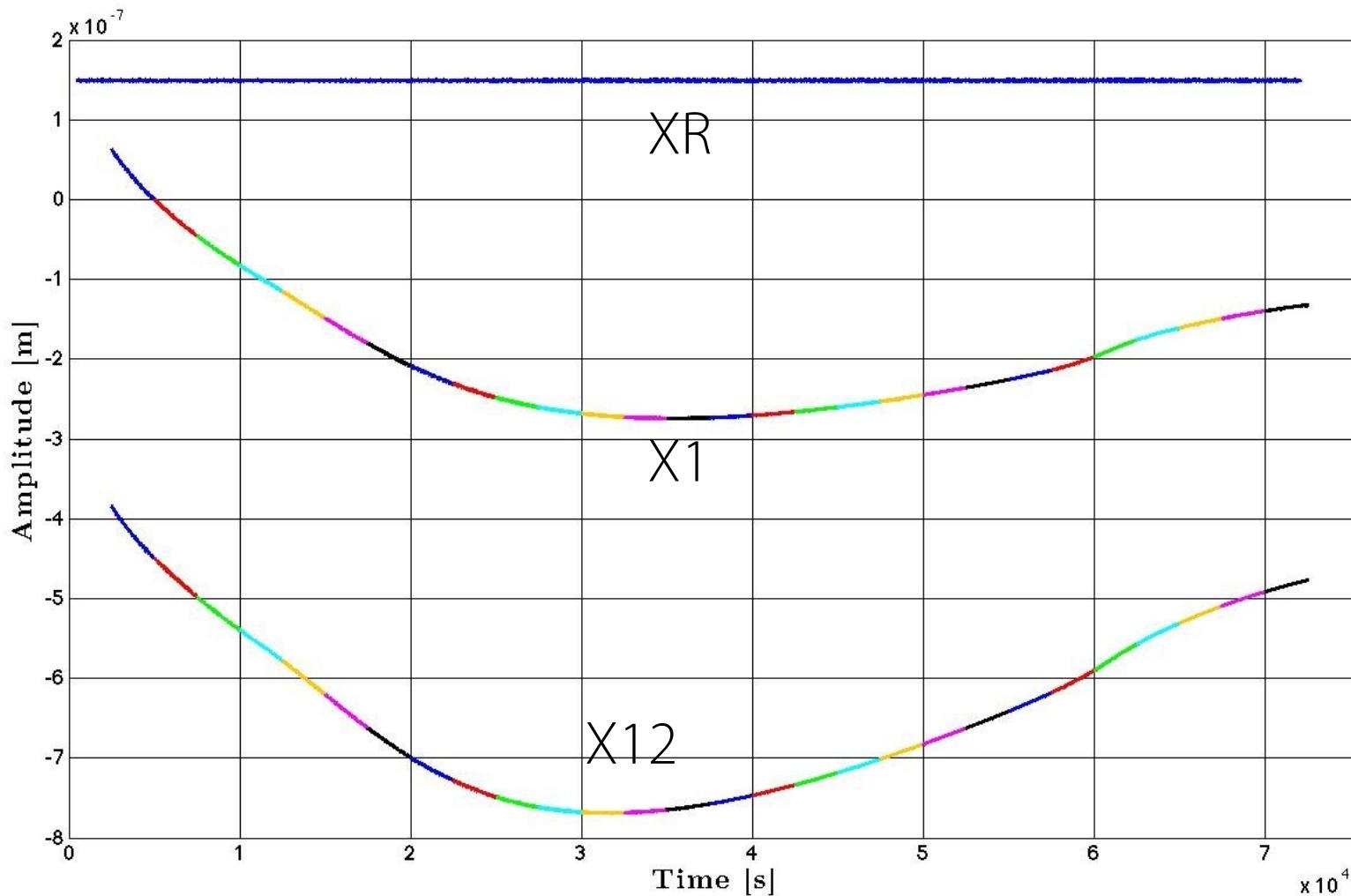


amplitude noise
phase noise



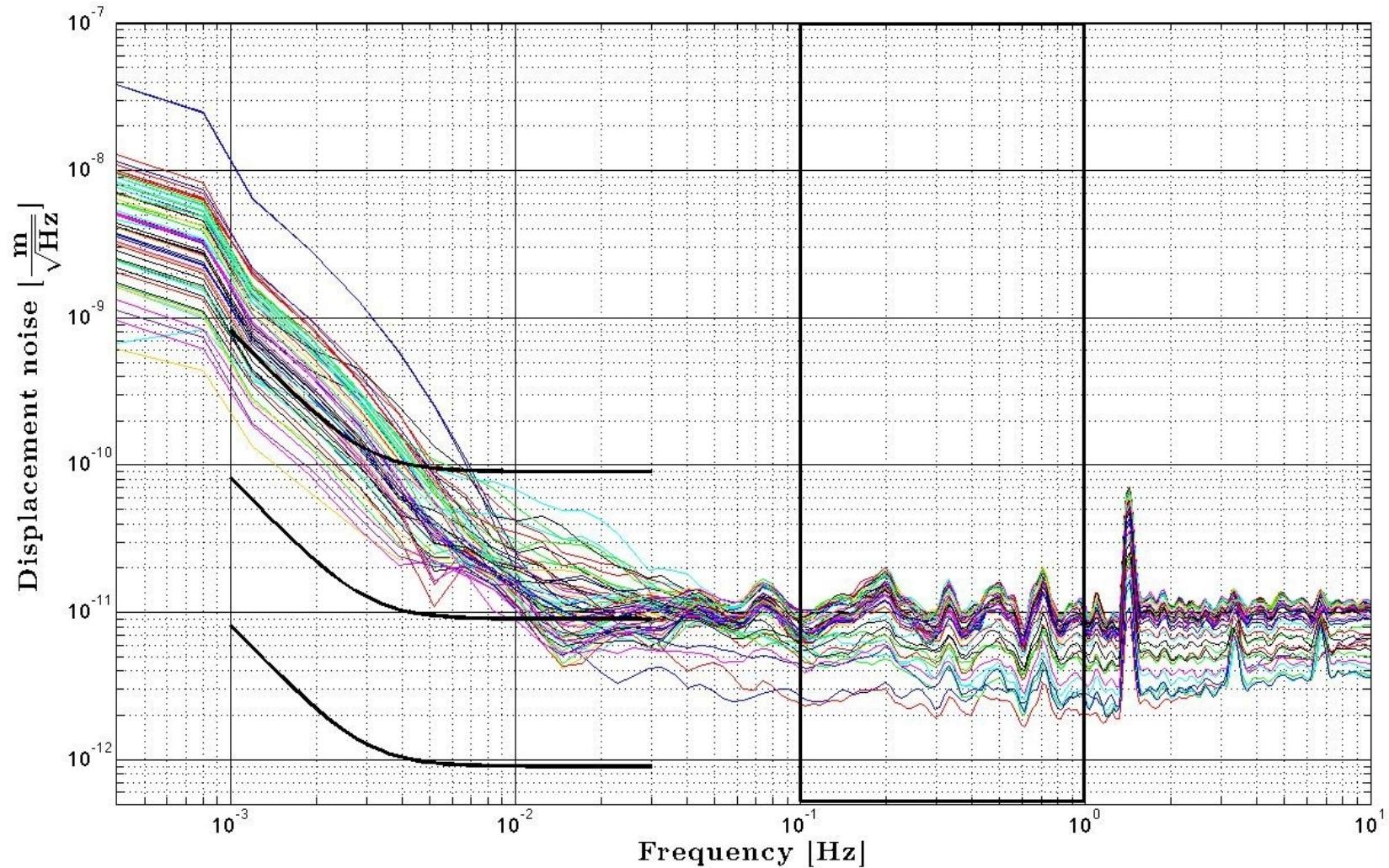


Experiment





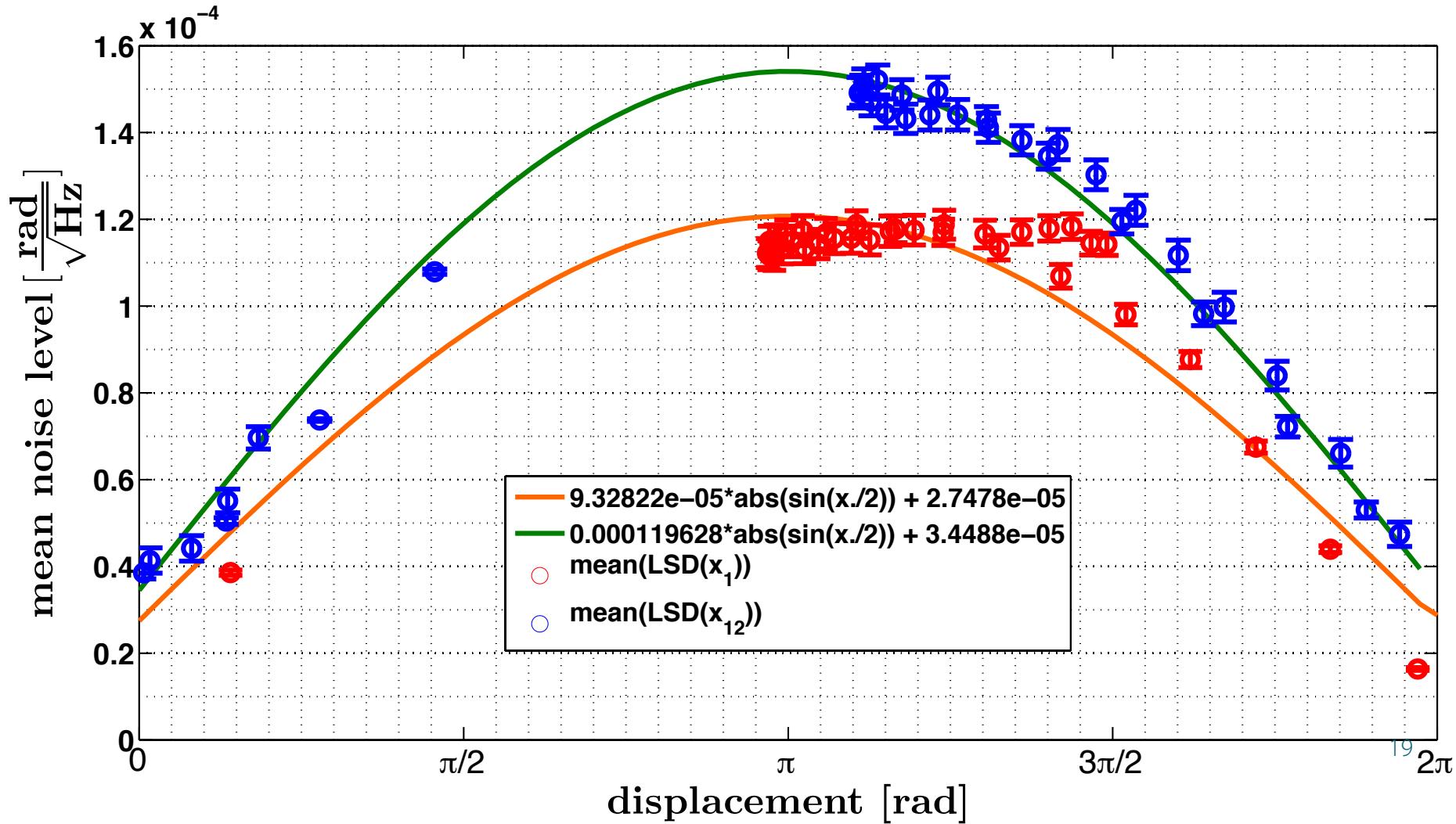
Experiment





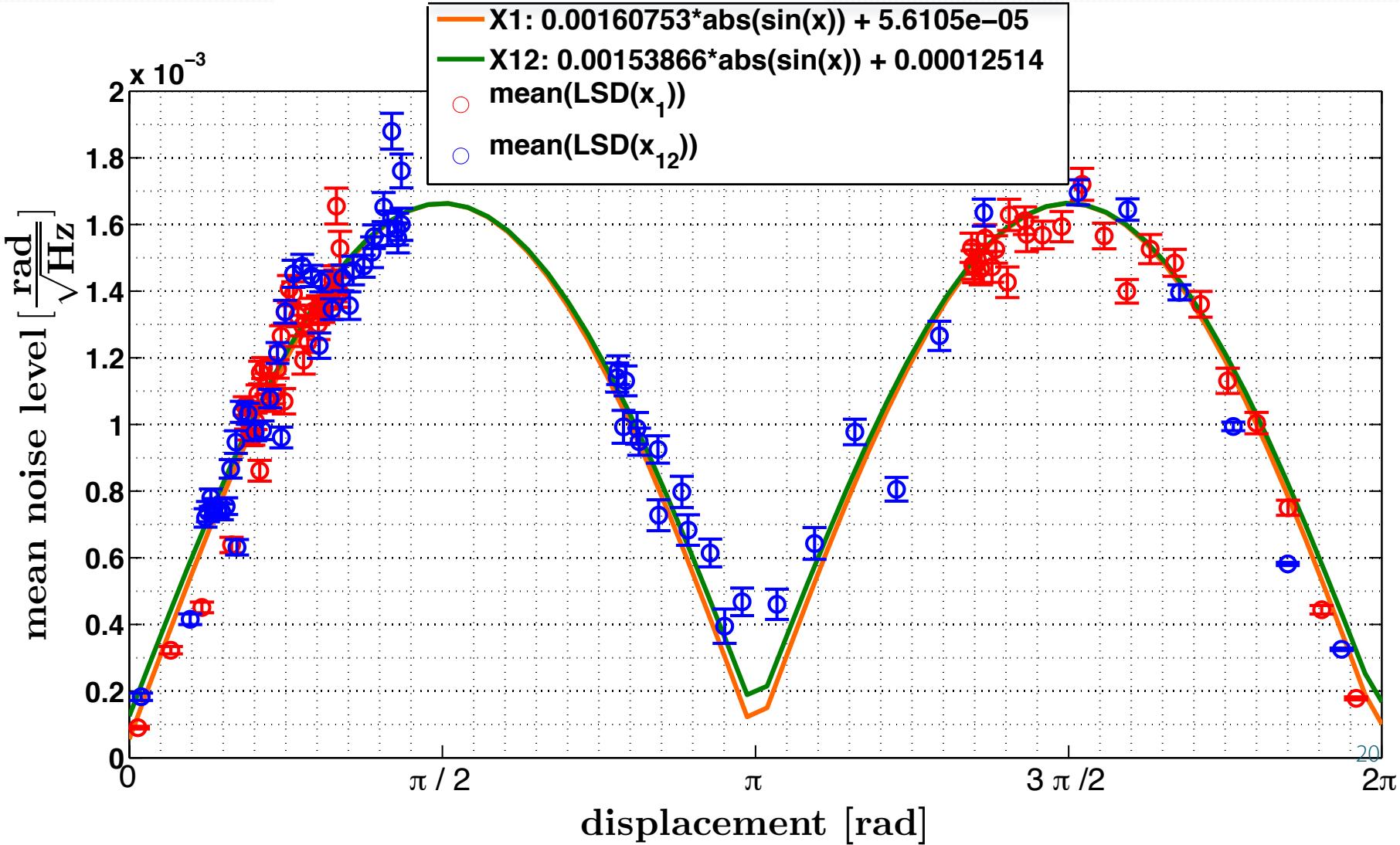
Measurements - amplitude noise

$$\langle \Delta n_{\text{an}}^2 \rangle = \frac{2}{NA_{\text{in}}^2} \langle n_k^2 \rangle 4 \sin^2 (\psi/2)$$



Measurements - phase noise

$$\Delta n_{\text{pn}} = \frac{2}{N} \langle n_k^2 \rangle \sin^2(\phi - \psi)$$

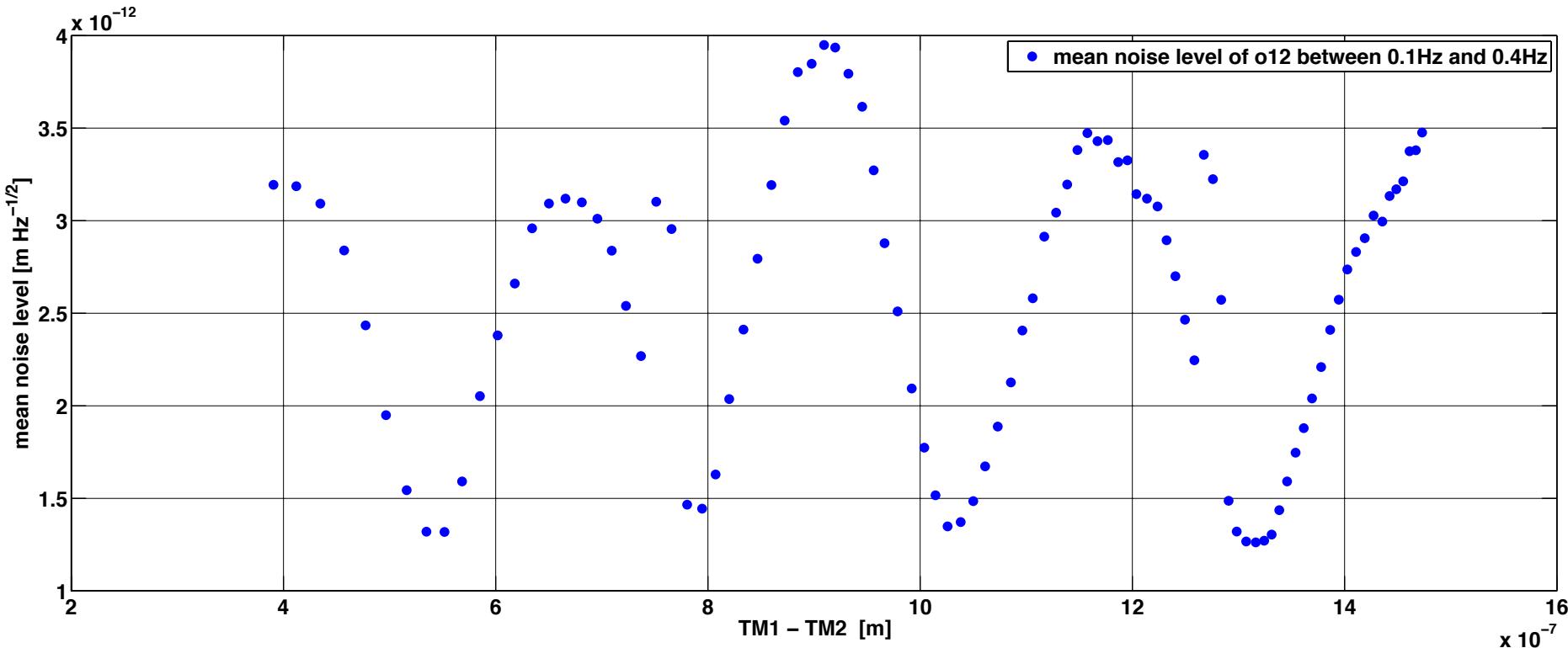




Measurements - phase noise

- LPF STOC SIM4

UTC





Outlook

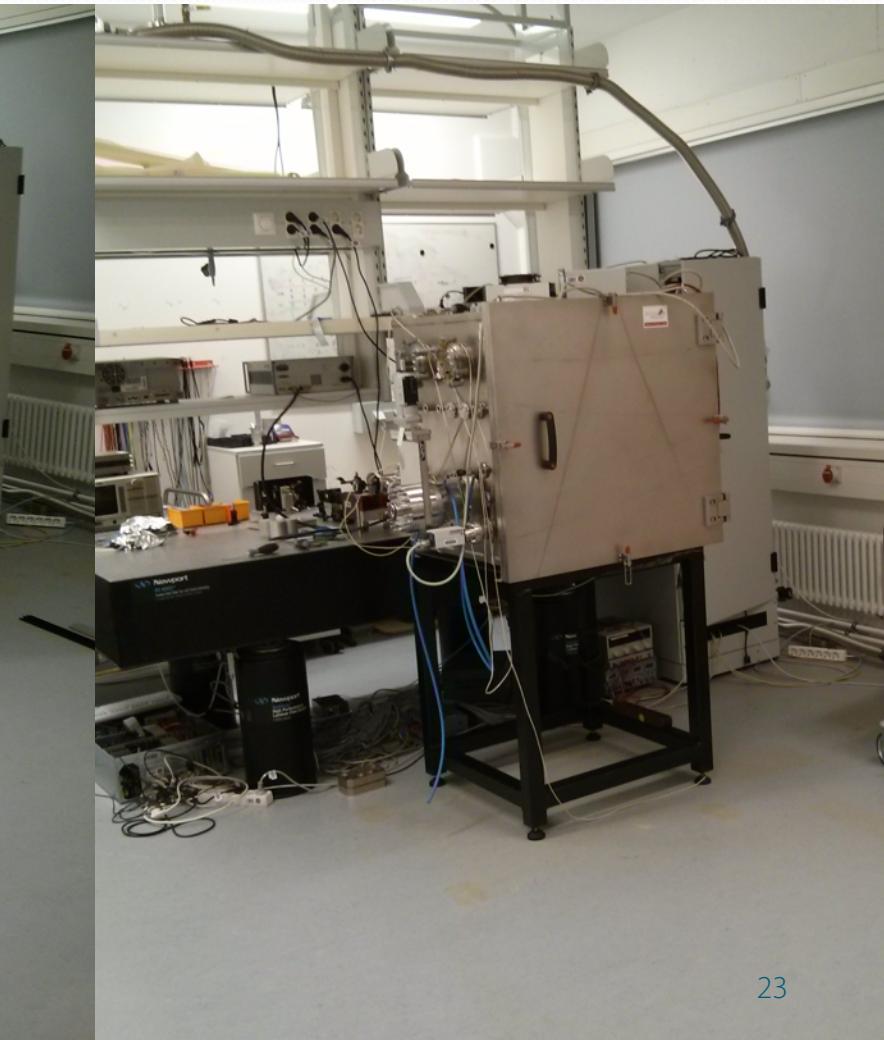
- new vacuum tank





Outlook

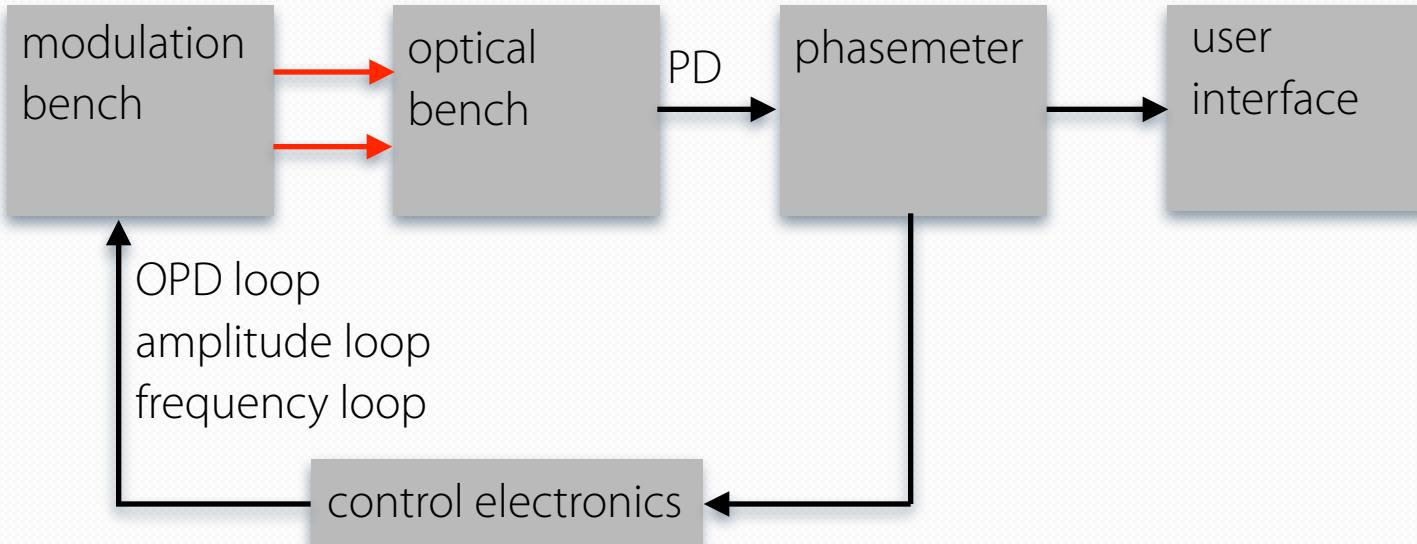
- new vacuum tank





Outlook

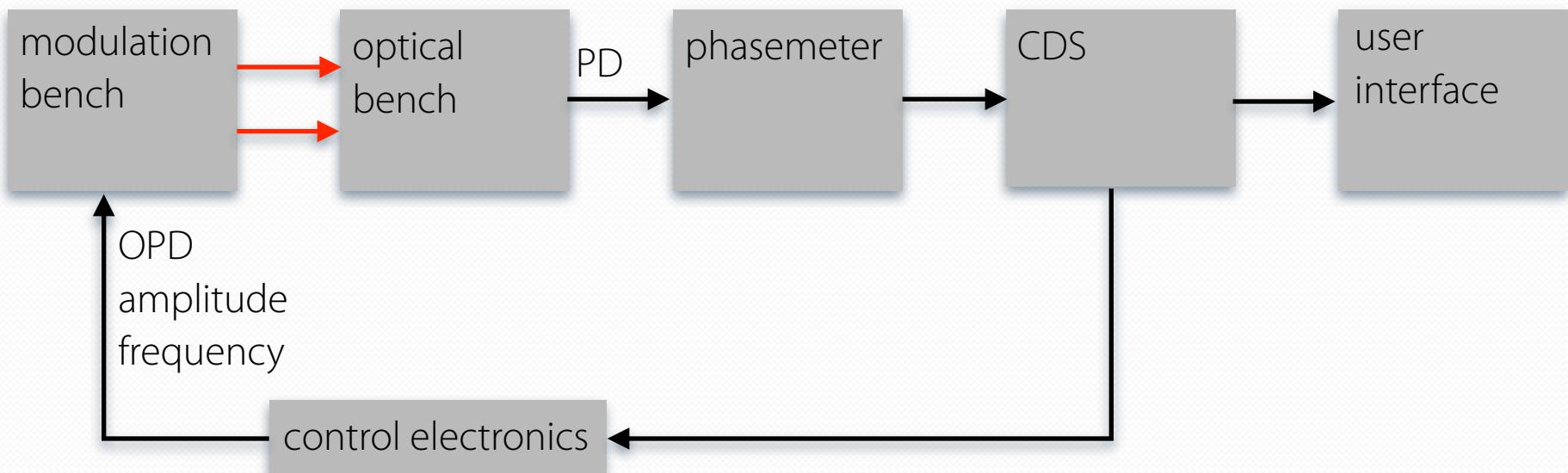
- new vacuum tank
- CDS system for phasemeter readout
- digital control and/or monitoring of control loops





Outlook

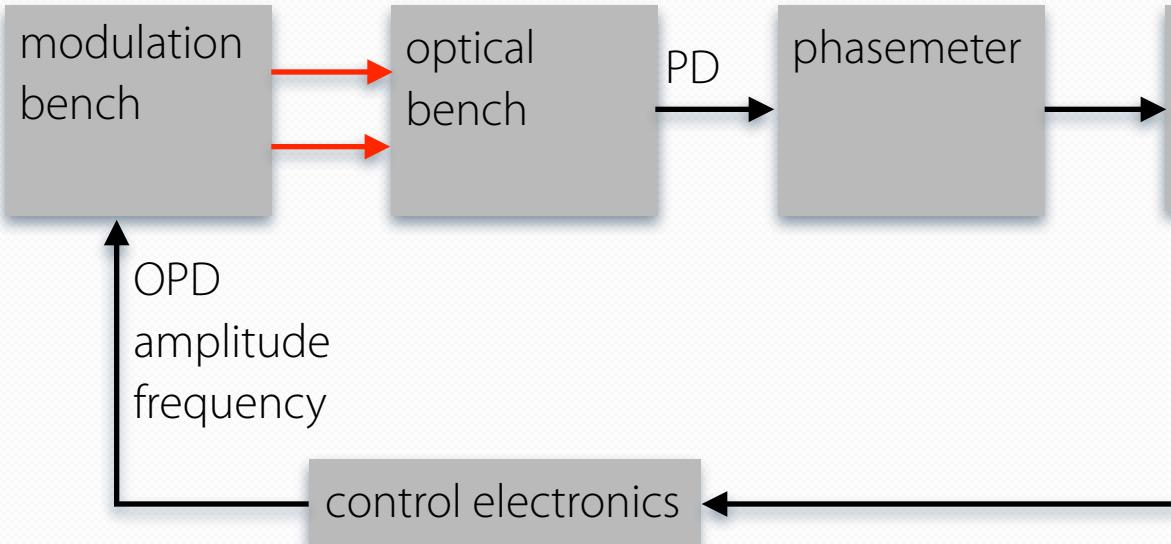
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Outlook

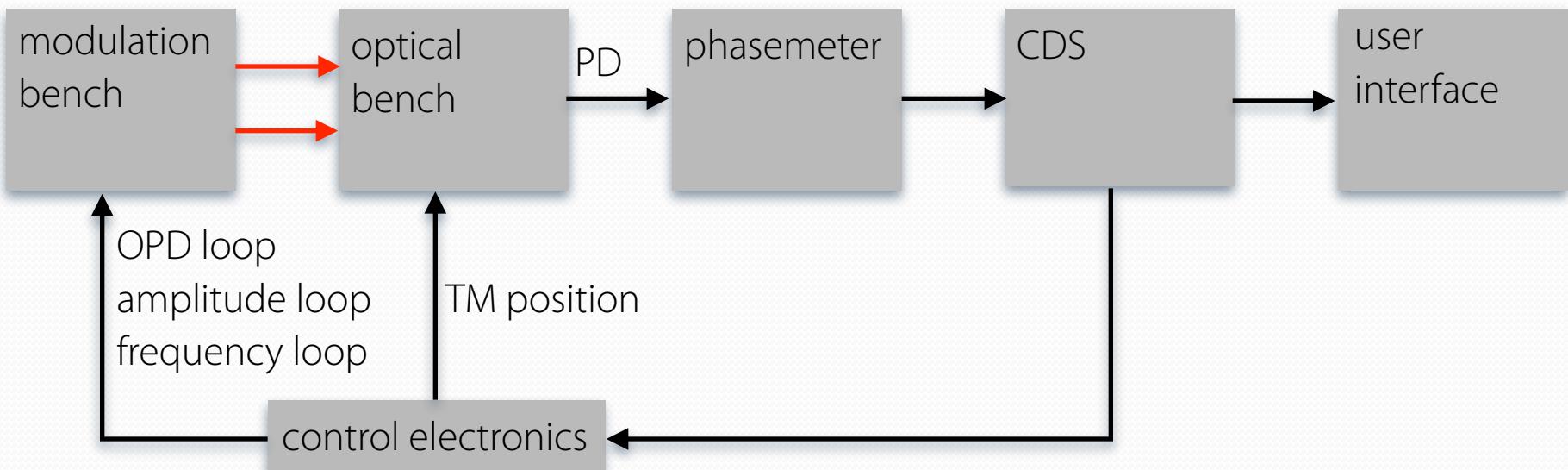
- new vacuum tank
- CDS system for phasemeter readout
- digital control and/or monitoring of control loops





Outlook

- new vacuum tank
- CDS system for phasemeter readout
- digital control and/or monitoring of control loops
- digital control of test mass mirror piezos





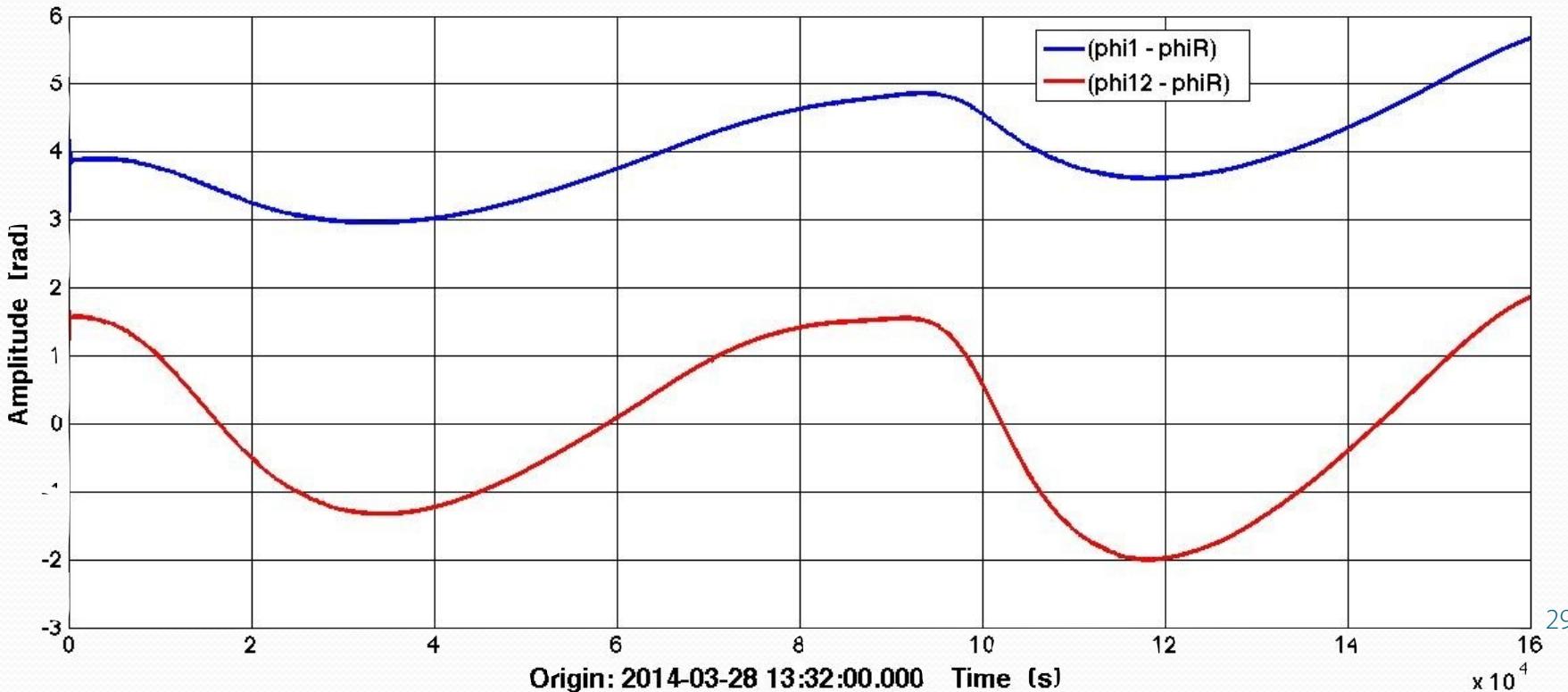
Outlook

- new vacuum tank
- CDS system for phasemeter readout
- digital control and/or monitoring of control loops
- digital control of test mass mirror piezos
 - adjustment of test masses while the tank is closed
 - low frequency test mass drift stabilisation



Outlook

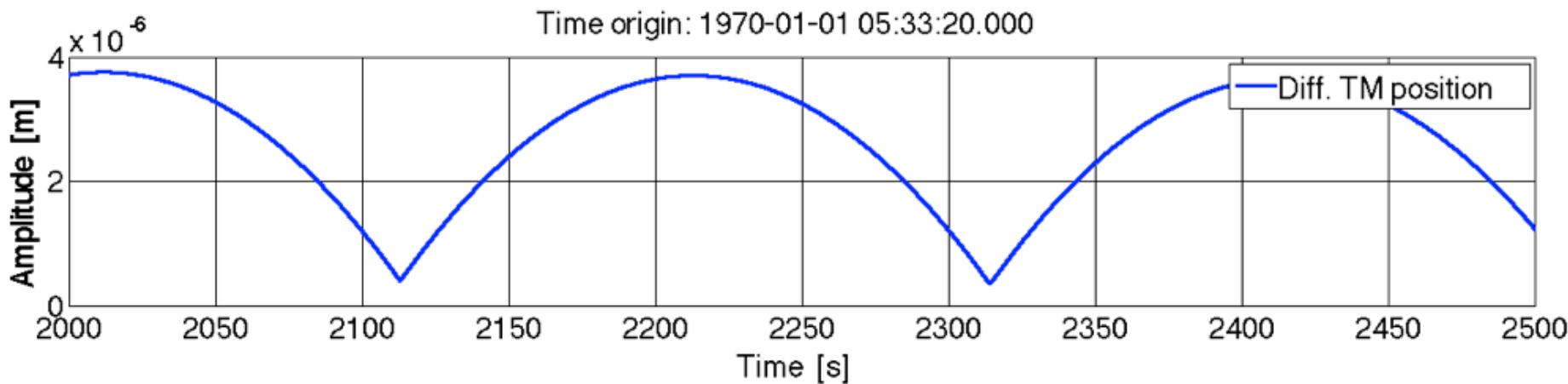
- new vacuum tank
- CDS system for phasemeter readout
- digital control and/or monitoring of control loops
- digital control of test mass mirror piezos





Outlook

- new vacuum tank
- CDS system for phasemeter readout
- digital control and/or monitoring of control loops
- digital control of test mass mirror piezos





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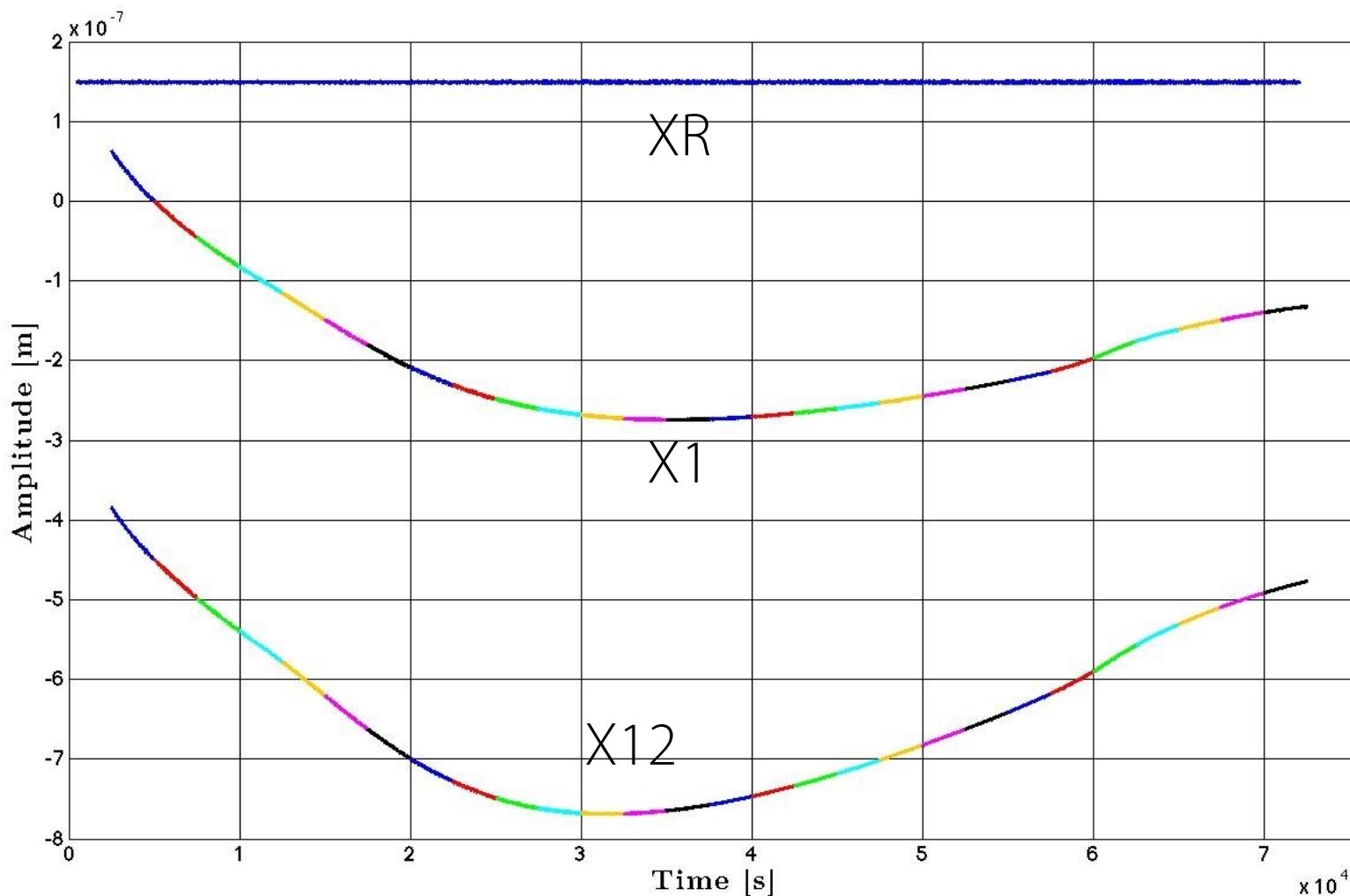
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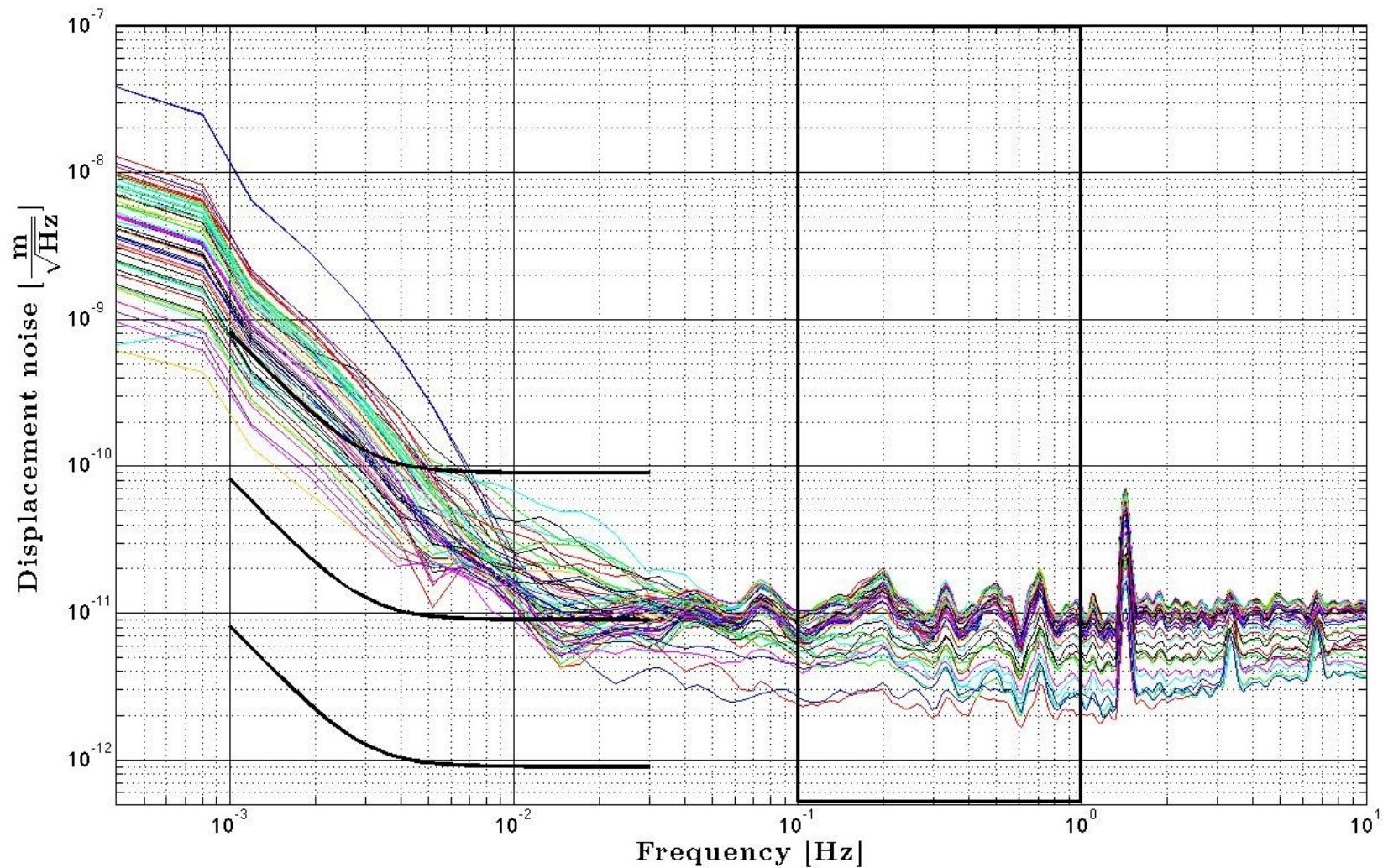
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extra - data analysis

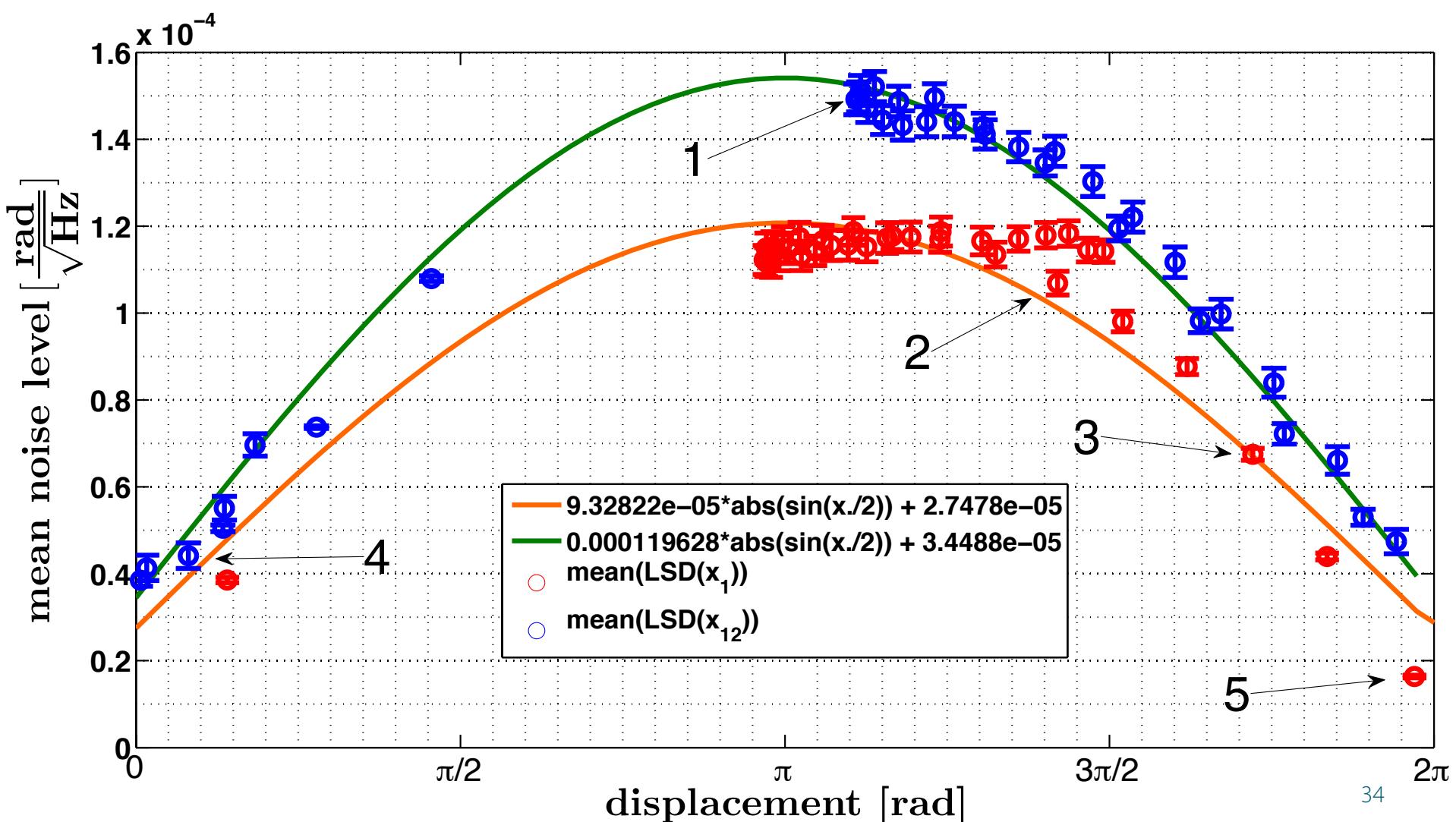




extra - data analysis

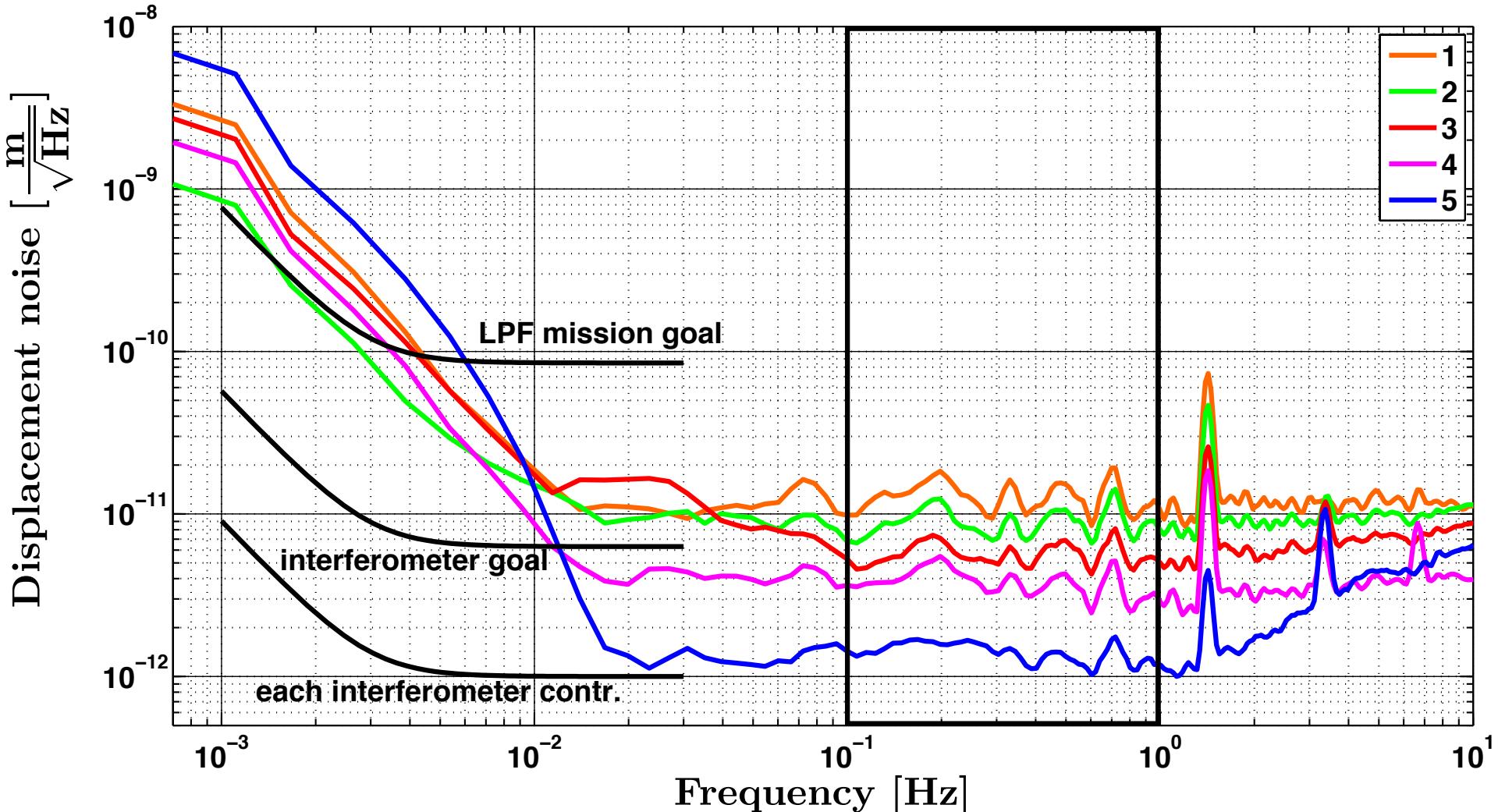


extra - amplitude noise



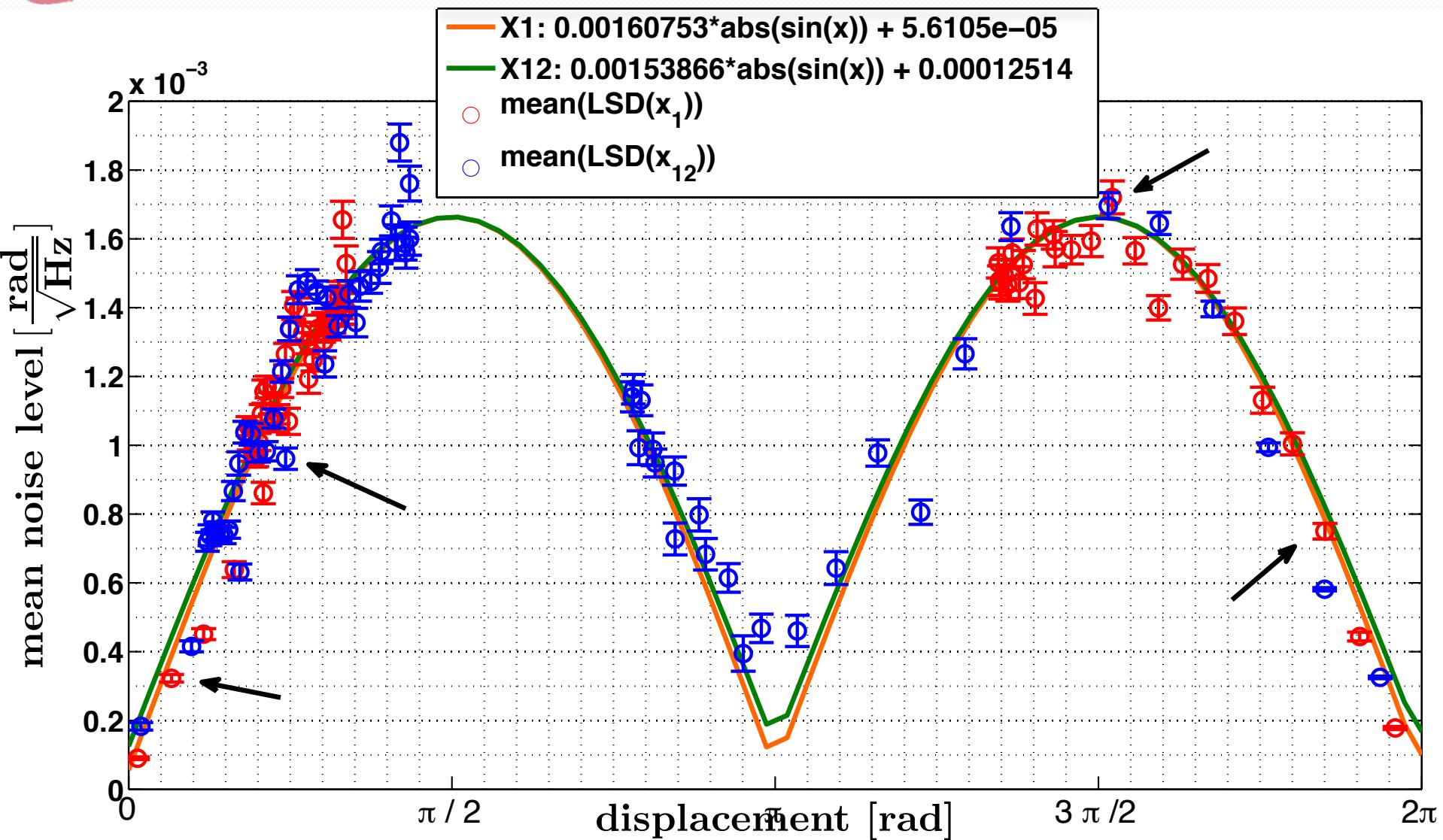


extra - amplitude noise





extra - OPD noise





extra - OPD noise

