





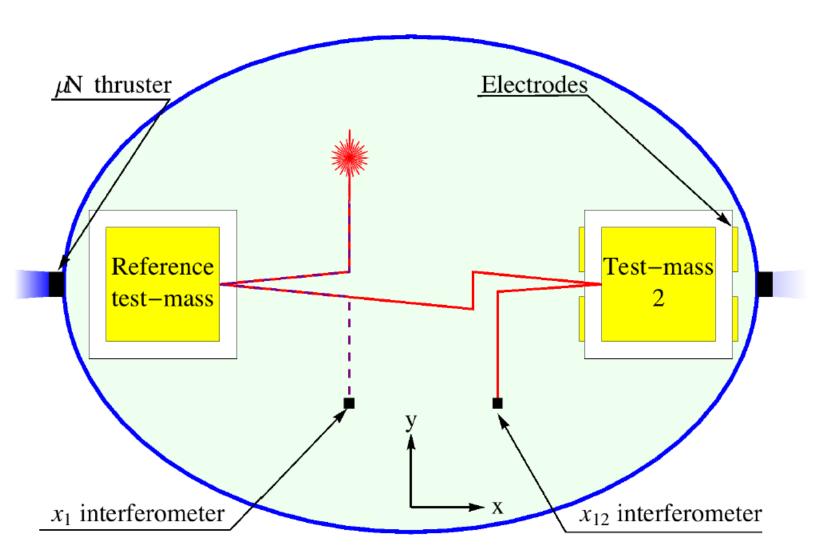
#### External force measurement in controlled dynamical systems with unknown noise: the case of LISA Pathfinder

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#### LISA Pathfinder (LPF)



#### LPF is a dynamical controlled system

Control loops should make the system to behave linear with a good approximation

$$\Delta a = \sum_{j} \frac{d^2}{dt^2} \left( S_j \ast x_j \right) - \sum_{j} \omega_j^2 \ast x_j + \sum_{j} A_j \ast g_j^c + \Delta g$$

- $x_j$ : signals like  $x_1$  or  $x_{12}$  (but also other dof)
- $S_j$ : pickup
- $\omega_i^2$ : stiffness and cross-stiffness
- $g_i^c$  : commanded forces by the control loops
- $A_i$  : converts  $g_i^c$  into "true" forces
- $\Delta g$  : external forces (also the noise of commanded forces)

#### The basics of LISA Pathfinder (LPF)

Main Goal:  $\Delta g$ 

**Requirements:** the square root of  $PSD(\Delta g)$  better than

$$\leq 3 \times 10^{-14} \sqrt{1 + \left(\frac{f}{3 \,\mathrm{mHz}}\right)^2} \,\mathrm{ms}^{-2} / \sqrt{\mathrm{Hz}}$$

over a frequency bandwidth of 1-30 mHz

- We need to:
  - characterize the disturbance noises of the instrument
  - subract the relative timeseries

#### **Conventional method**

- Frequency domain
- Solve the equation of motion
- Derive the transfer function

 $x_i(\omega) = H_{ij}(\omega) \Delta g_j(\omega) (+x_{i,free-evolution}(\omega))$ 

• Invert and get  $\Delta g_j(\omega)$ 

#### **Conventional method**

• Drawbacks:

– We need the solution of the dynamics  $\ddot{x} = g$ 

- We need to know very well the control law

$$\ddot{x} = g + g_{feedback}$$

Free-evolution term

$$x(t) = \int_0^\infty t' g(t - t') dt' + v_0 t + x_0$$

#### The case of LPF

- We want to measure  $\Delta g$  at low frequency (1-30 mHz)
- We have a controlled dynamical system
- We do not need to solve the equation of motion but just to fit it!
- We have all the timeseries of position and commanded force (from the telemetry)

## Fitting the acceleration

- Solution of dynamics not required
- No transients from the free-evolution (annoying at low frequencies)
- We can subtract forces directly (read or measured)
- Spourious force spikes are spikes within the force dataseries

## Fitting the acceleration

- We should have an a priori estimation of the noise;
- However, in signal-dominated experiment (as eLISA) it is not so easy;
- In this case, noise is one of the output of a global signal search procedure;
- In LPF, noise is the main scientific goal!

## Applying to the case of LPF

The residual could be written as

$$\Delta \tilde{a}\left[k\right] - \sum_{j=1}^{N_g} \Delta \tilde{g}_j\left[k, \vec{\theta}\right] = \Delta \tilde{g}_{noise}\left[k\right]$$

 ~ indicates Discrete Fourier Transform (DFT) that means

$$\Delta \tilde{g}_i[k] = \frac{1}{\sqrt{N_d}} \sum_{n=0}^{N_d - 1} \Delta g_i[n] w[n] e^{-i n k \frac{2\pi}{N_d}}$$

- w is the spectral window (Blackmann-Harris)
- N<sub>d</sub> is the number of data

#### The new loglikelihood

• Instead of maximizing

$$\Lambda\left(\vec{\theta}\right) = -N_s \sum_{k \in Q} \frac{\left|\Delta \tilde{g}_{noise}\left[k, \vec{\theta}\right]\right|^2}{s_k} + C'$$

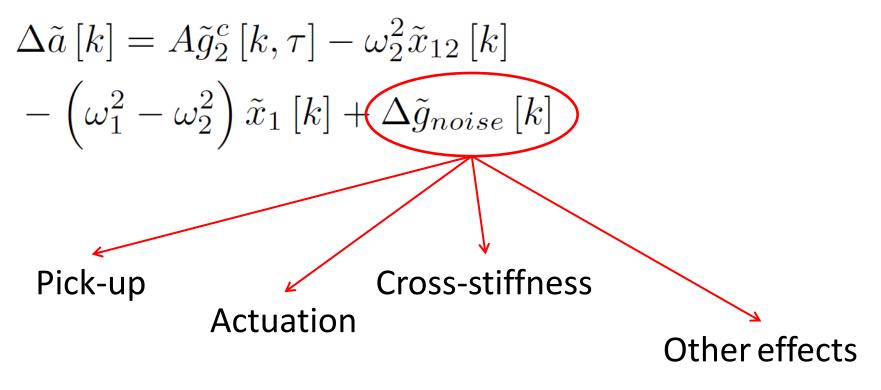
we can maximize (after noise marginalization)

$$\Lambda\left(\vec{\theta}\right) = -N_s \sum_{k \in Q} \log\left(\left|\Delta \tilde{g}_{noise}\left[k, \vec{\theta}\right]\right|^2\right) + C$$

arXiv:1404.4792v1, S. Vitale, D.V. et al.

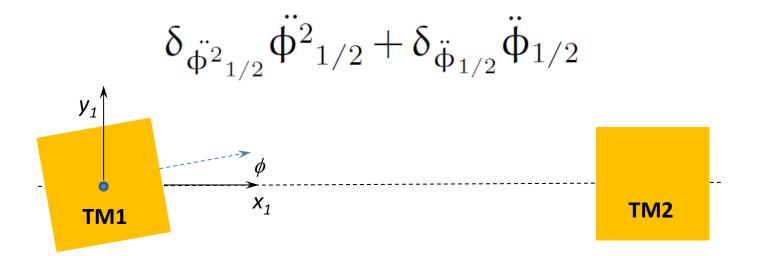
#### The Crosstalk Experiment What are we talking about?

• What we think is pure noise, actually contains some signal we could try to subtract



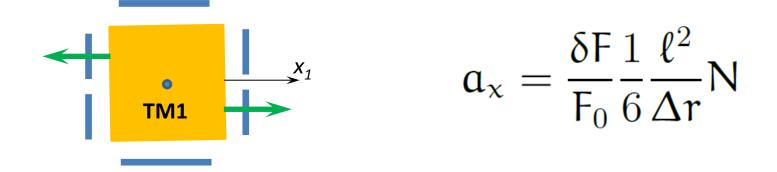
#### The pick-up

The piston effect (linear and non linear)



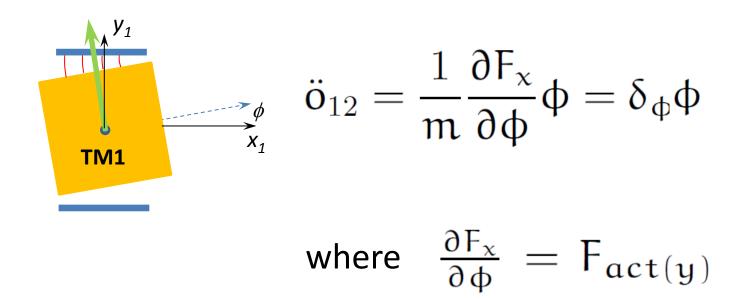
#### The actuation crosstalk

#### The torque-into-acceleration effect



#### The cross-stiffness

Projection of force gradients from other dof



#### The crosstalk on the xy-plane

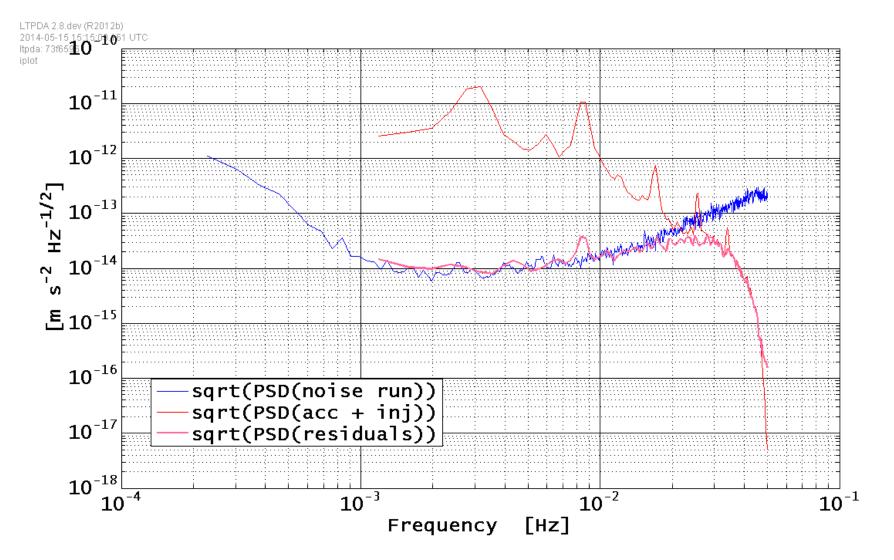
- Inject a guidance signal into the control loop of  $\phi_1$
- Measure the readout of the differential interferometer
- Fit the our data to the equation of crosstalk for the  $\varphi_1$  injection

$$\begin{aligned} \Delta a &= -\delta_{\ddot{\varphi}_1} \ddot{\varphi}_1 + \delta_{\varphi_1} \varphi_1 + \delta_{\ddot{\varphi}_1^2} \ddot{\varphi}_1^2 - \delta_{\mathsf{N}_{\mathsf{cmd}},\varphi_1} \mathsf{N}_{\varphi_1} - \omega_2^2(\mathsf{x}_{12} + \mathsf{x}_1) + \\ &+ \omega_1^2 \mathsf{x}_1 - \mathcal{A}_{\mathsf{sus}} \mathsf{f}_{\mathsf{cmd}}, \mathsf{x}_2 + \delta_{\ddot{\delta}y} (\ddot{y}_1 - \ddot{y}_2) + \Delta g \end{aligned}$$

# $\phi_1$ injections – Results

Param	Units	Noise	Unknown Noise	mechanism
$\delta_{\ddot{\varphi}_1}$	m/rad	$(1.37 \pm 0.003) \times 10^{-4}$	$(1.37 \pm 0.003) \times 10^{-4}$	Linear Piston
$\delta_{\varphi_1}$	m/s <sup>2</sup> rad	$(-6.5 \pm 0.1) \times 10^{-10}$	$(-6.6 \pm 0.2) \times 10^{-10}$	Cross-stiffness $\omega_{\phi x}^2$
$\delta_{\ddot{\Phi}_1^2}$	$m/rad^2$	$-0.19 \pm 0.24 \times 10^{-6}$	$-0.19 \pm 0.06 \times 10^{-6}$	Non-linear piston
$\delta_{N_{cmd, \varphi 1}}$	m	$(-2\pm3)\times10^{-7}$	$(-2\pm3)\times10^{-7}$	Torque imbalance
$\omega_2^2$	$1/s^2$	$(-2.14 \pm 0.06) \times 10^{-6}$	$(-2.14 \pm 0.06) \times 10^{-6}$	Stiffness TM2
$\omega_1^2$	$1/s^2$	$(-2.01 \pm 0.37) \times 10^{-6}$	$(-2.01 \pm 0.37) \times 10^{-6}$	Stiffness TM1
A <sub>sus</sub>	no units	1.05	1.05	Gain of the suspension
τ	S	$0.226 \pm 0.002$	$0.222 \pm 1.141 \times 10^{-10}$	delay of the OBC
δ <sub>äy</sub>	rad	$-0.00035 \pm 0.00004$	$-0.00035 \pm 0.00004$	non-orthogonality of TM faces

#### The PSD of the residual noise



#### The search for GW with eLISA

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#### Space-borne gravitational-wave detectors as time-delayed differential dynamometers

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- eLISA will scan the GWs sky at very low frequency (0.1 mHz – 1 Hz)
- It is signal dominated (we hope!)
- Data analysis should be performed in this framework (fit in acceleration with unknown noise)

#### Conclusions

- Fit in acceleration to subtract force noise
- Use the new likelihood to fit with a priori unknown noise
- The procedure was tested with LPF Simulator and Torsion pendulum: it works!
- GWs as tidal forces allows to use in eLISA data analysis