

TES III Workshop
Gainesville, FL, 17-18 August 2006

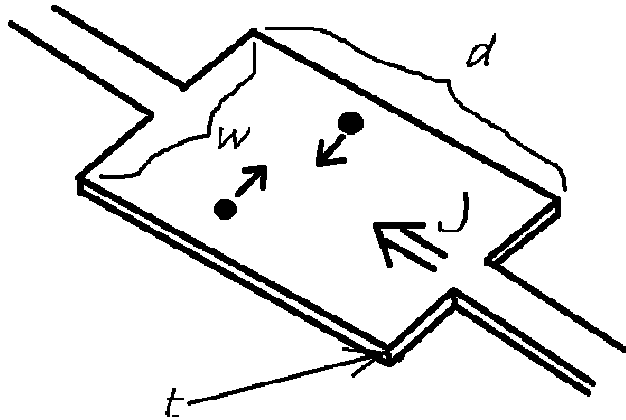
Flux Flow noise in Transition Edge Sensors



Massimiliano Galeazzi



Review of Flux Flow Noise



ALL expressions are in SI units

v	=	vortex speed
η	=	viscosity
ϕ_0	=	flux quantum
J	=	current density
μ_0	=	magnetization of vacuum
H_{C2}	=	critical field
ρ_n	=	normal state resistivity
V_1	=	voltage generated by one vortex
V	=	voltage
I	=	current
N	=	average number of vortices
V_{RMS}	=	voltage noise root mean square
τ	=	vortex average lifetime
B	=	noise bandwidth
$S(f)$	=	noise power density
e_{ff}	=	noise spectral density
l	=	vortex effective mean free path
V_o	=	"correlation" voltage

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vortices move perpendicular to current flow with speed:

$$v = \frac{\phi_0 J}{\eta}$$

where

$$\eta = \frac{\phi_0 \mu_0 H_{C2}}{\rho_n} \cdot$$

Each vortex generates a voltage

$$V_1 = \frac{v \phi_0}{w} = \frac{\phi_0 \phi_0 J}{w \eta} = \frac{\phi_0}{w} \phi_0 J \frac{\rho_n}{\phi_0 \mu_0 H_{C2}} = \frac{\phi_0}{\mu_0} \frac{I \rho_n}{w d H_{C2}}$$

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If the resistance at the transition is completely due to flux flow motion

$$\rightarrow R = \frac{V}{I} = \frac{NV_1}{I}$$

$$\rightarrow N = \frac{RI}{V_1} = \frac{\mu_0 R}{\phi_0 R_n} w^2 H_{C2}$$

For SMALL N this generates a RMS voltage noise:

$$V_{RMS} = \sqrt{N} \cdot V_1 = \sqrt{RIV_1}$$

The average lifetime of each vortex is give by

$$\tau = \frac{w}{v}$$

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$$\rightarrow B = \frac{1}{\tau} = \frac{v}{w}$$

$$\rightarrow S(f) = \frac{V_{RMS}^2}{B} = \frac{RIV_1}{v/w} = \phi_0 V$$

$$\rightarrow e_{ff} = \sqrt{\phi_0 V}$$

This is the same result obtained by Knoedler and Voss [Phys. Rev. B 26, 449 (1982)] assuming "vortex" shot noise.

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Review of Flux Flow Noise

ISSUE #1: The observed noise is too small
 → Introduction of vortex mean free path

$$\rightarrow B = \frac{1}{\tau} = \frac{v}{l}$$

$$\rightarrow S(f) = \frac{V_{RMS}^2}{B} = \frac{RIV_1}{l} = \phi_0 V \frac{l}{w}$$

$$\rightarrow e_{ff} = \sqrt{\phi_0 V \frac{l}{w}}$$

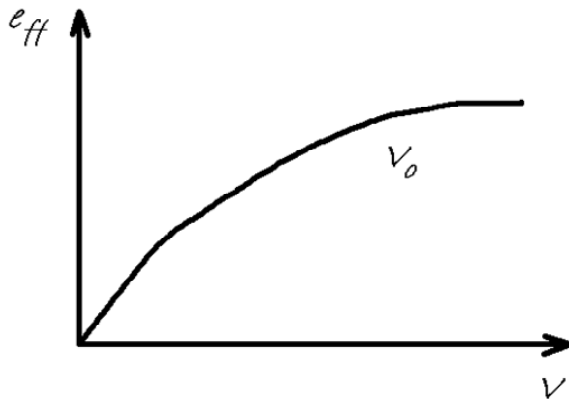
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Review of Flux Flow Noise

ISSUE #2: For large N the vortices are correlated
→ e_{ff} is smaller

But $N = \frac{V}{V_1}$ → for large voltage the noise is reduced due to the correlation (saturation effect).



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Review of Flux Flow Noise

FIRST ORDER APPROXIMATION:

Replace V with $\frac{V}{1 + V/V_0}$, where $V_0 = \text{const.}$

(dependent on V_1)

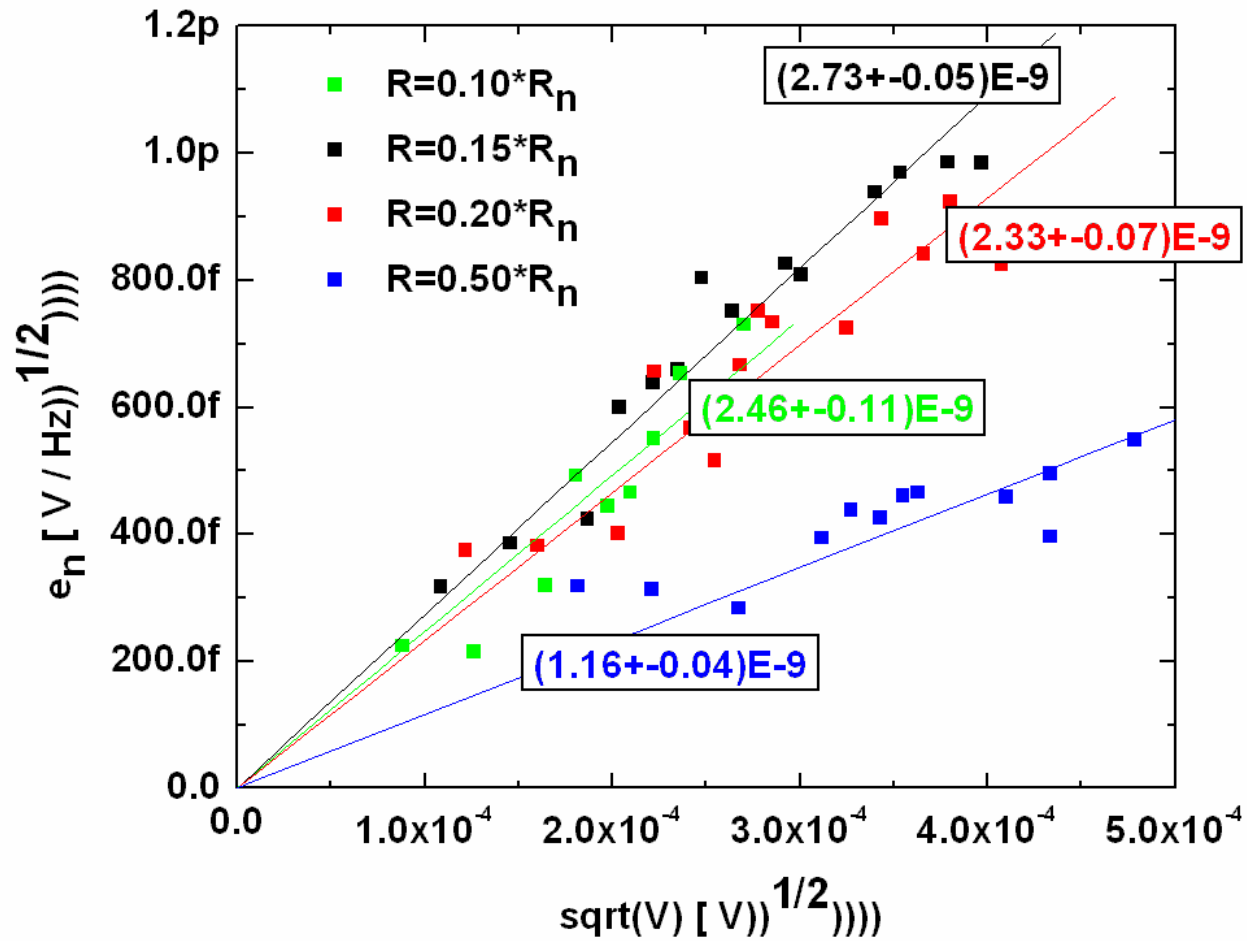
$$\rightarrow e_{ff} = \sqrt{\phi_0 \frac{V}{1 + V/V_0} \frac{l}{w}}$$

$$\text{for } V \ll V_0 \quad \rightarrow \quad e_{ff} = \sqrt{\phi_0 V \frac{l}{w}}$$

$$\text{for } V \gg V_0 \quad \rightarrow \quad e_{ff} = \sqrt{\phi_0 V_0 \frac{l}{w}}$$

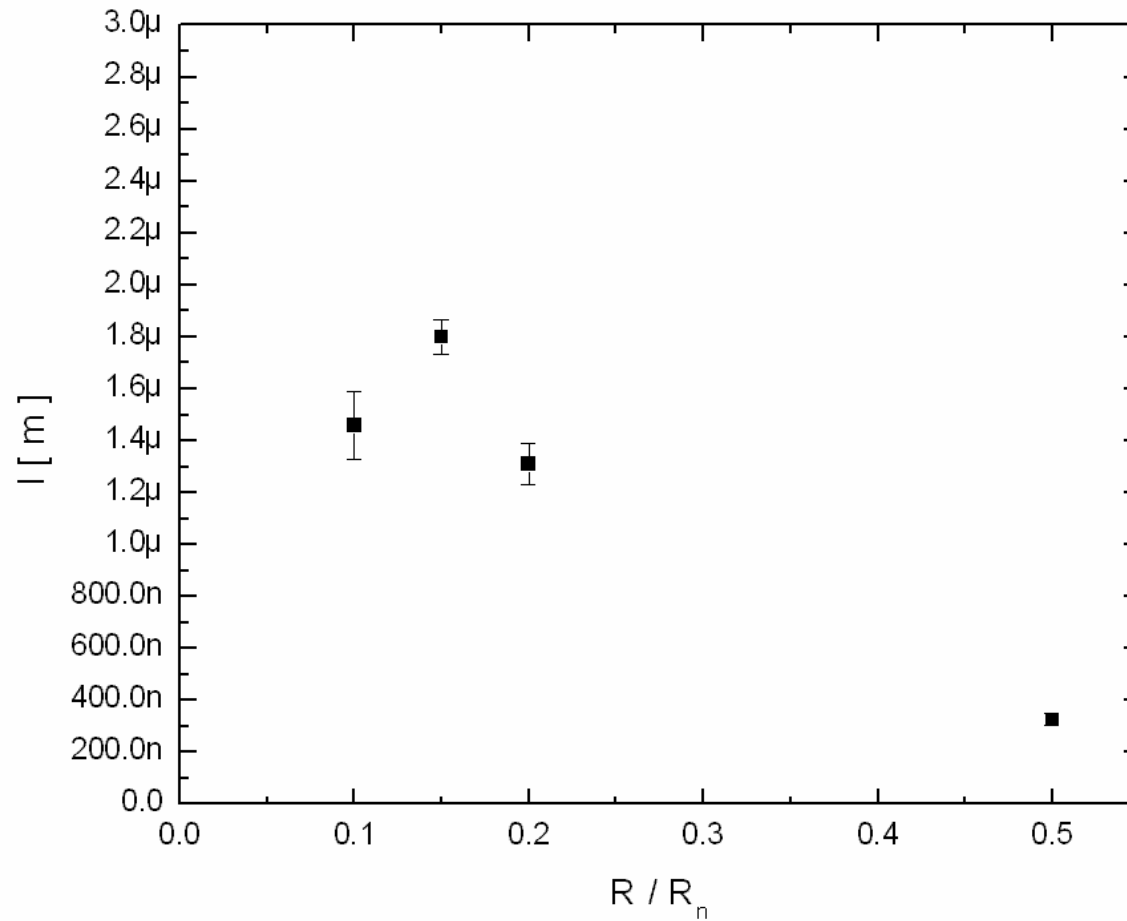
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Experimental evidence

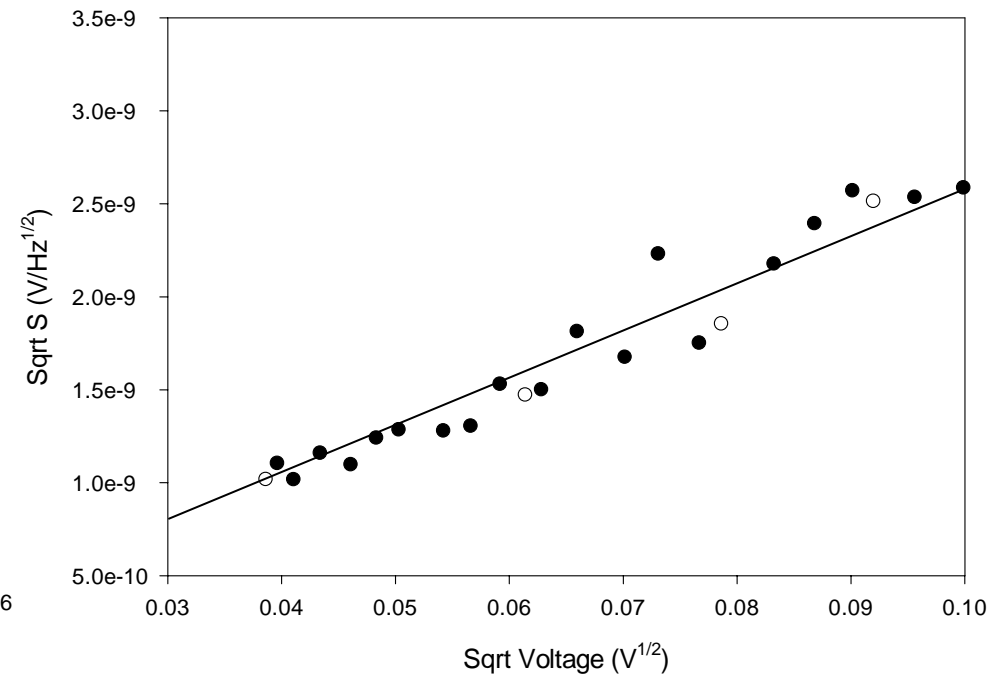
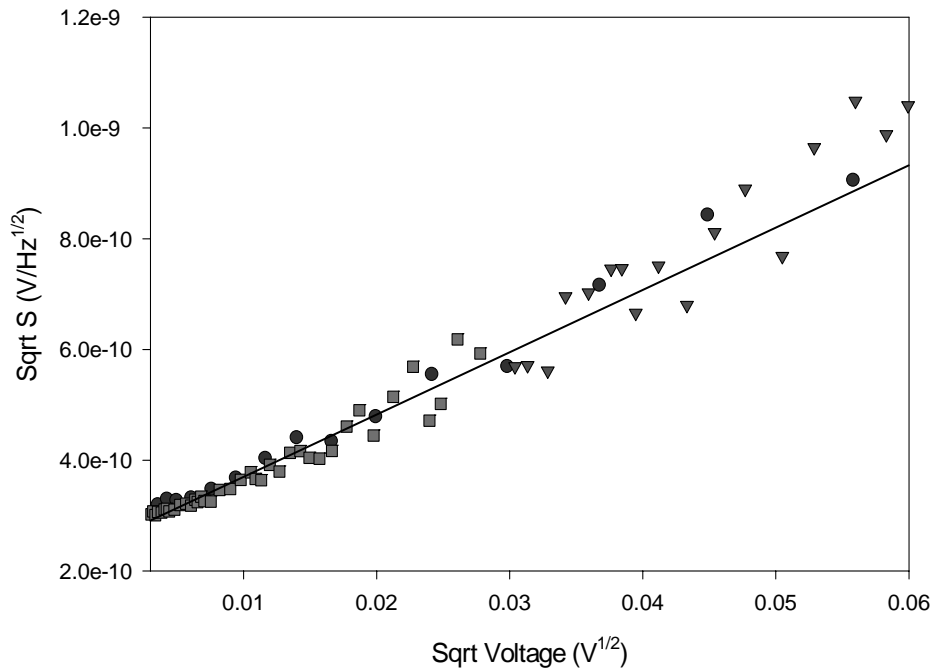


Data courtesy of the X-ray Astrophysics group at the NASA/GSFC

Mean Free Path



Experimental Evidence





Open Questions

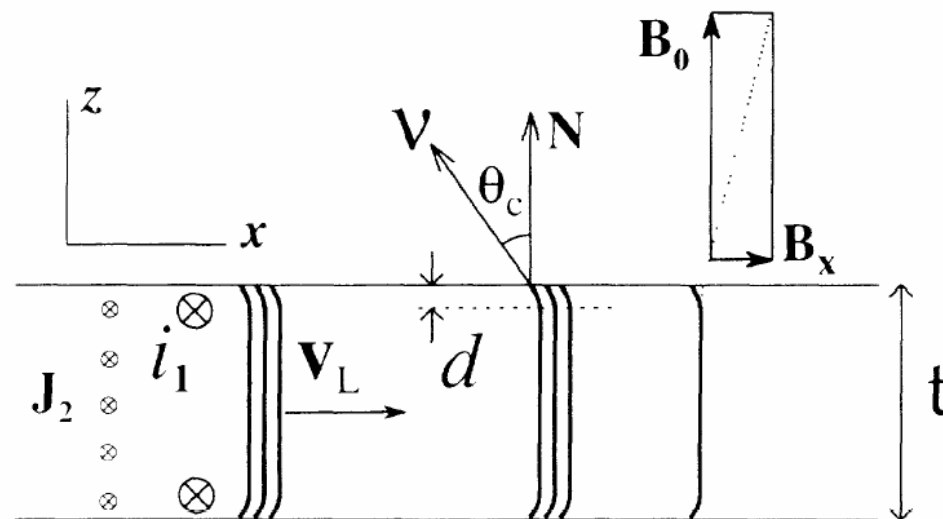
- What is the mean free path l ?
- Why do we have a dependence of the noise on α ?

→ Different Approach to Flux Flow Noise

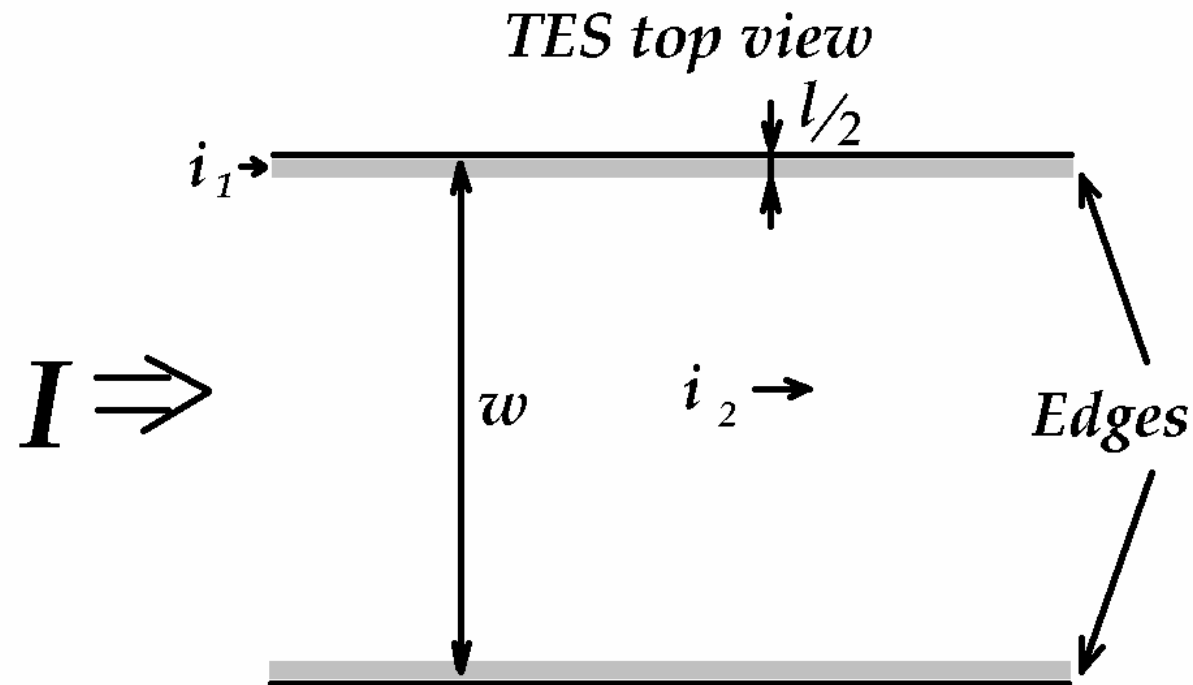
Flux Flow Noise Revisited

Placais, Matheiu, and Simon, PRB 49, 15815 (1994)

1. A 3D treatment is necessary
2. In the film there are two separate currents contributions: a non-dissipative current at the edges and a dissipative current in the bulk
3. The non-dissipative current at the edges is of the order of the critical current i_c (A/cm)
4. It is the non-dissipative term that generates the noise



Flux Flow Noise Revisited



i_1 = non-dissipative current per unit width

$i_1 \sim i_c$ (critical current per unit width)

i_2 = dissipative current per unit width

$$\rightarrow I = i_1 \cdot l + i_2 \cdot w \sim i_2 \cdot w$$

U Flux Flow Noise Revisited

Flux Flow Model

$$S(f) = \frac{V_{RMS}^2}{B} = \frac{RIV_1}{w} = \phi_o V$$

$$e_{ff} = \sqrt{\phi_o V}$$

Flux Flow Model Revisited

$$\begin{aligned} S(f) &= \frac{V_{RMS}^2}{B} = \frac{R(i_1 l)V_1}{w} = \\ &= \frac{R(i_1 l)V_1}{w} \cdot \frac{I}{I} = \frac{RIV_1}{w} \cdot \frac{(i_1 l)}{I} \approx \phi_o V \frac{i_1 l}{i_2 w} \end{aligned}$$

$$e_{ff} = \sqrt{\phi_o V \frac{i_1 l}{i_2 w}} \approx \sqrt{\phi_o V \frac{i_C \cdot l}{i \cdot w}}$$

Detector sensitivity α

$$E_J = \frac{\hbar I_C}{2e}$$

Energy to break vortexes

$$k_B T_{KT} \sim E_J$$

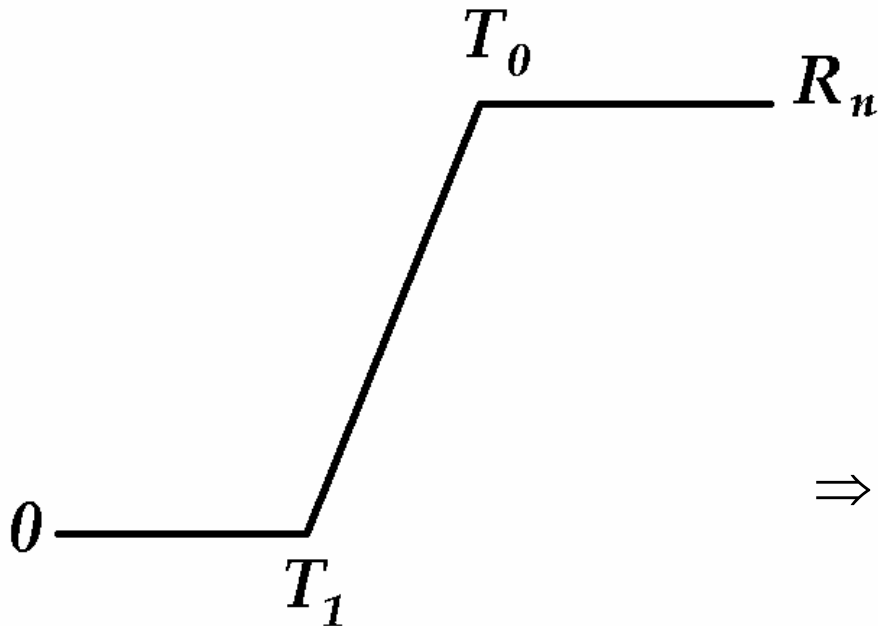
Kosterlitz-Thouless Transition Temperature

$$T_{KT} \sim T_0$$

For low Resistance (Beaseley and Mooji, 1979)

$$k_B T_1 = E_J - E \approx kT_0 - E$$

E = Energy provided by current (or magnetic field)



$$\Rightarrow \Delta T = T_0 - T_1 = \frac{E}{k_B} \approx T_0 \frac{E}{E_J}$$

$$\Rightarrow \alpha = \frac{T}{R} \cdot \frac{\Delta R}{\Delta T} \sim \frac{T_0}{R} \cdot \frac{R_n}{T_0 \frac{E}{E_J}} = \frac{R_n}{R} \frac{E_J}{E} \propto \frac{I_C}{I}$$

Flux Flow Noise Revisited

$$e_{ff} \approx \sqrt{\phi_0 V \frac{l}{w} \alpha}$$