



LOW TEMPERATURE TRANSFORMER READOUT ELECTRONICS  
Flavio Gatti

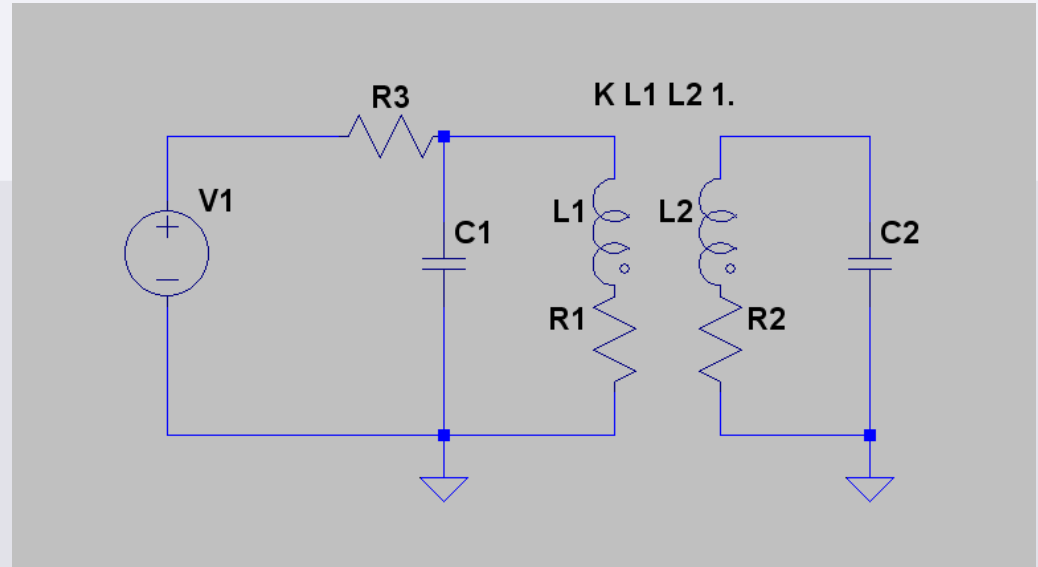
UNIVERSITY and INFN  
of Genoa, Italy

Luigi Parodi, Maria Ribeiro Gomes, Lorenza Ferrari, Riccardo Valle, Simeone Dussoni, Adriano Bevilacqua, Davide Bondi

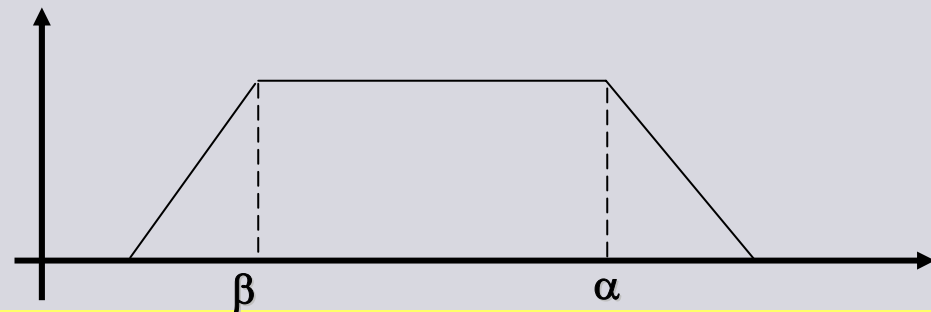
# Introduction

- After some very preliminary test presented in LTD11, we fixed a few results on the use of transformers as passive elements for matching TES and conventional electronics.
- Not a new Idea (already used in the past)
- New -> Investigation for a very high noise performance and for a reliable circuital solutions for TES operation.
- Our work has been dedicated specifically to the DC operation with Voltage Bias at low frequency (10KHz).
- AC operation extension are under course (see MAX's talk) and very High-Frequencies seems to open new scenarios.

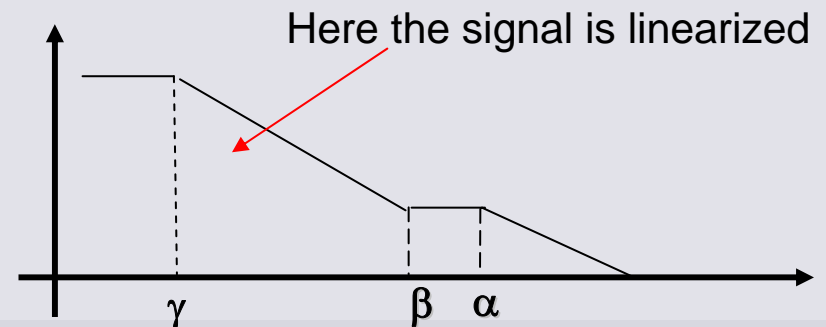
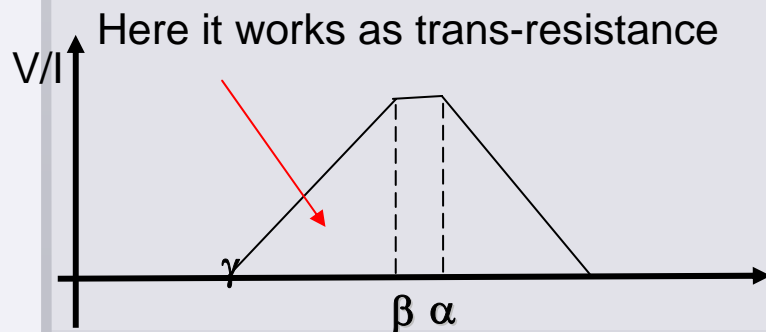
- Principle of operation



- $F(s) = n \tau \omega_0^2 [(s+\alpha)(s+\beta)]^{-1}$
- $\omega_0 = [L_s C]^{-1}$  ;  $\tau = L_p / R_{TES}$  ;  $M = [L_s L_p]^{1/2}$
- $\alpha = \tau \omega_0^2$  ;  $\beta = \tau^{-1}$

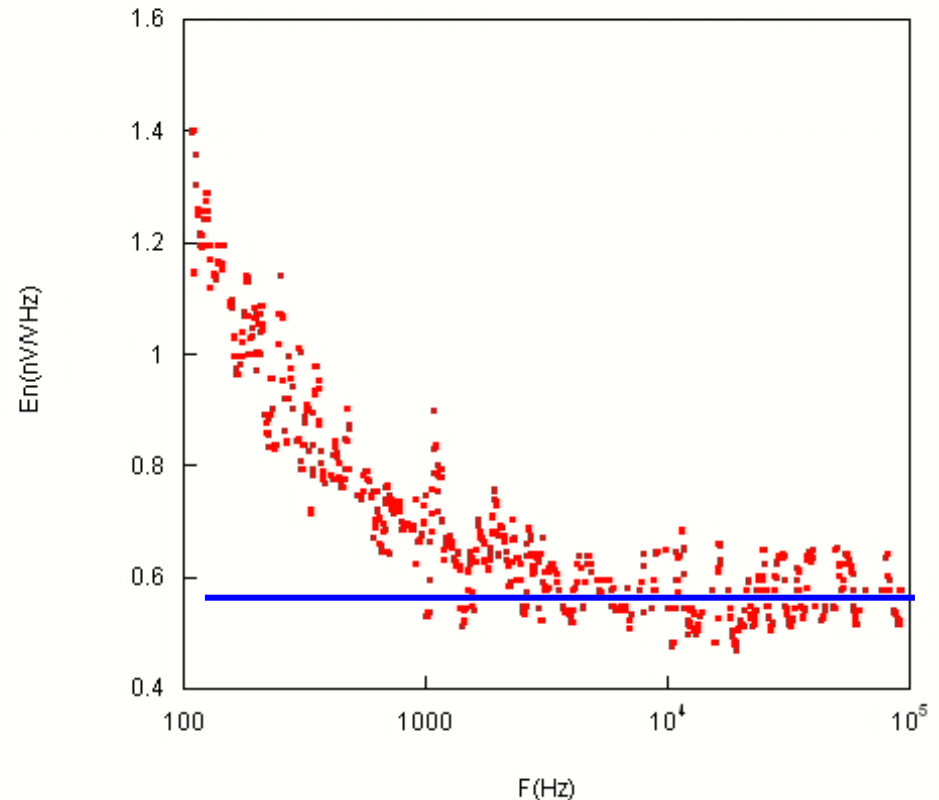


- Need to work in voltage BIAS  $\rightarrow Z_{TES} > Z_{Lp}$
- Current signal is transferred at frequencies  $< \beta$
- Increase  $\beta$  to cover detector bandwidth (10 KHz)
- Being  $L_p$  of typical transformer for low frequencies application at level of tenths of  $\mu\text{H}$ ,  $Z_{TES} = 0.1-1 \Omega$

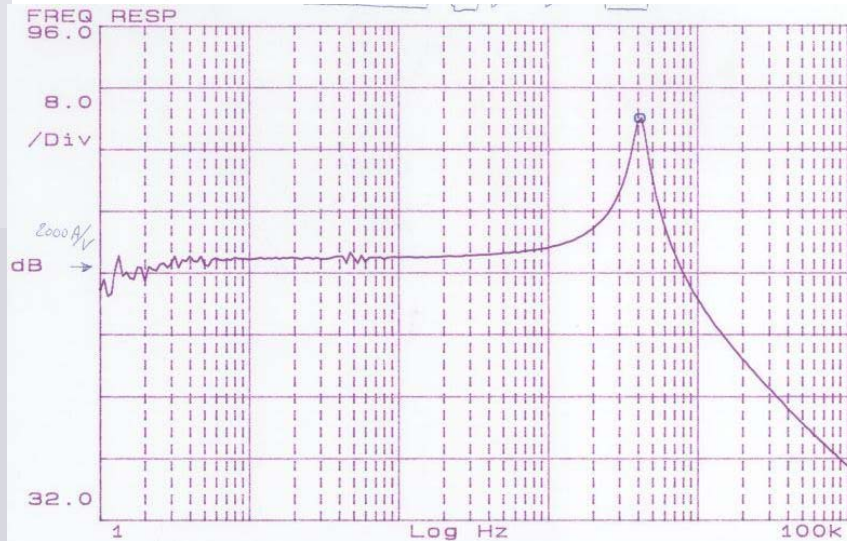
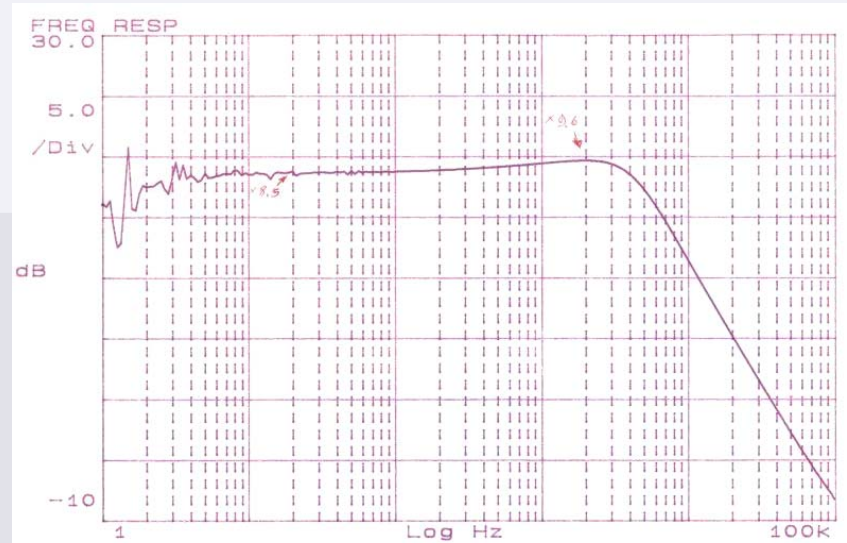
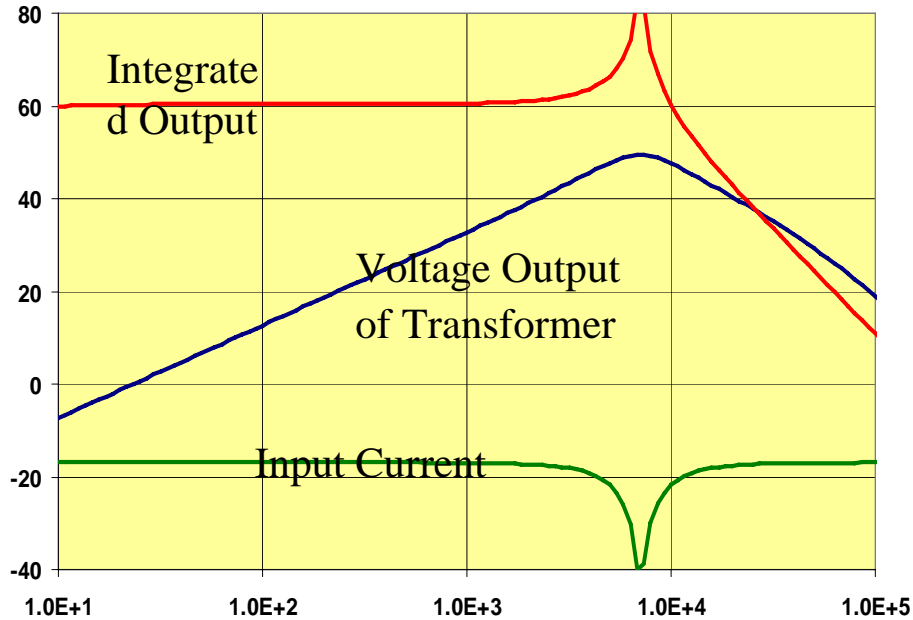


- Need of integration amplifier like Hi-Fi Amplifier for the pick-up coil signal

- The choice of the transformer is imposed by the noise performance of the amplifier
- We used room temperature amplifiers with 0.6 nV/VHz
- Transf. gain in the range 300–900 (turns ratio)
- High  $\mu$  core and capability to work in 0.1–4 K range.
- Transformer is on the Mix-Chamber, few cm from TES.



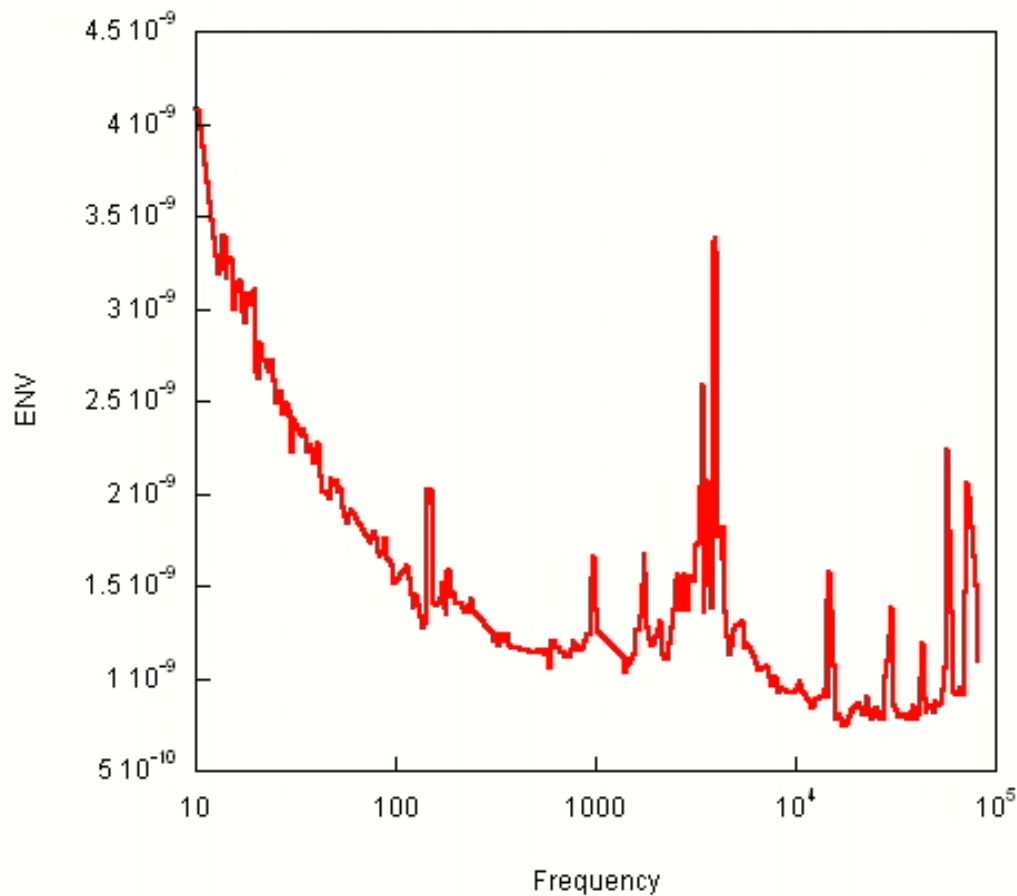
■ Simulated and measured Transfer Functions



## Transf Core selection

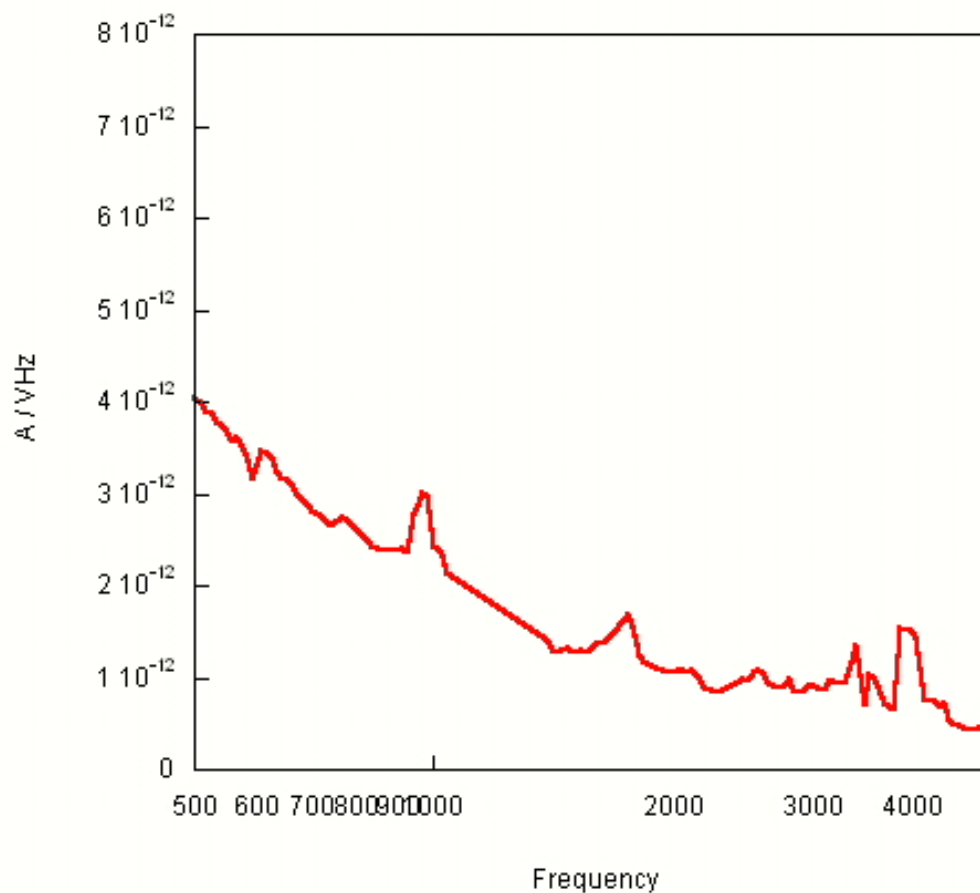
Core	$F_{\max}$ 300K	$F_{\max}$ 77K	$\theta$ (77K)	$\mu_{77}/\mu_{300}$	$\mu_4/\mu_{300}$	Exc noise
Met.glass	>100Khz	>100Khz	89.6	76%		yes
“	>100Khz	>100Khz	80.8	77%		yes
“	9.6KHz	19Khz	80.0	64%		yes
Mu-metal	31 Hz	282 Hz	80.0	50%		huge
“	20 Hz	58 Hz	80.0	73%		huge
ferrite	>100Khz	>100Khz	83.0	8%		yes
“	57Khz	>100Khz	81.0	6%		yes
“	>100Khz	51Kz	80.0	84%	82%	yes
spinglass	10.8Khz	9.63KHz	80.0	84%	50%	no
Unknown	>100Khz	>100Khz	88.4	99%		small
“	>100Khz	>100Khz	86.0	93%		small

- Noise spectrum from  $1 \Omega$  at Low T. Minimum detectable signal when R is at 25mK, about  $1.4 \text{ pA}/\sqrt{\text{Hz}}$ .

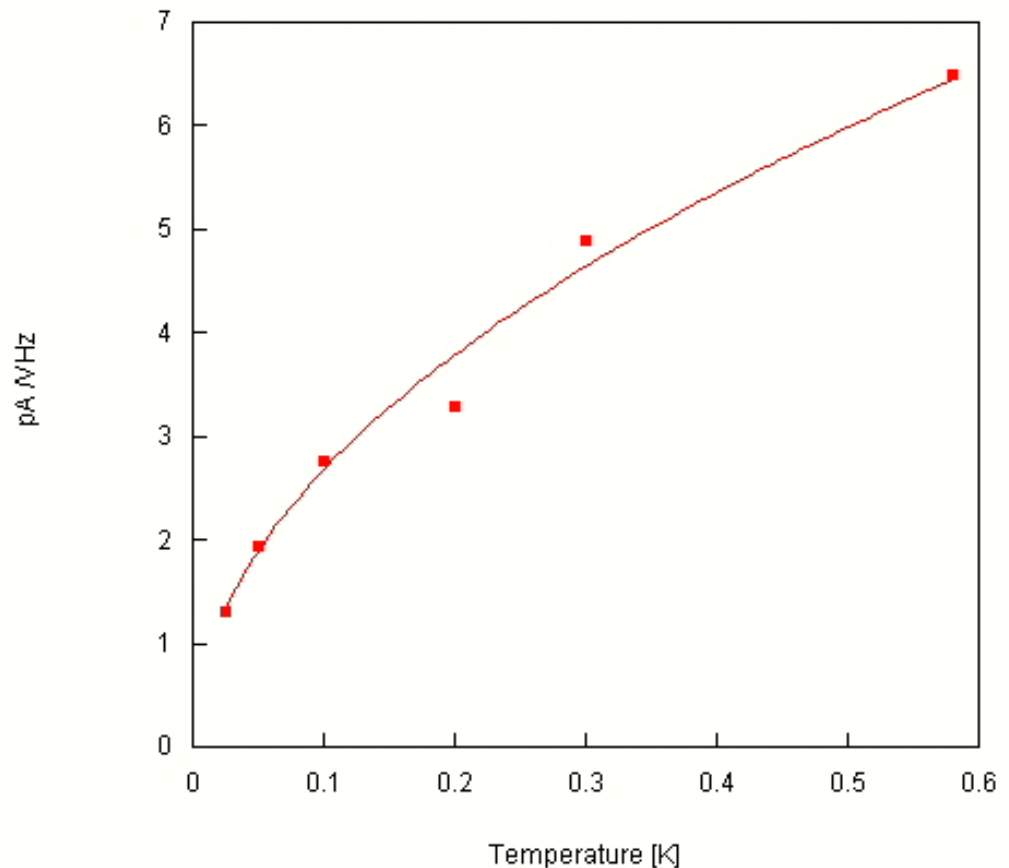




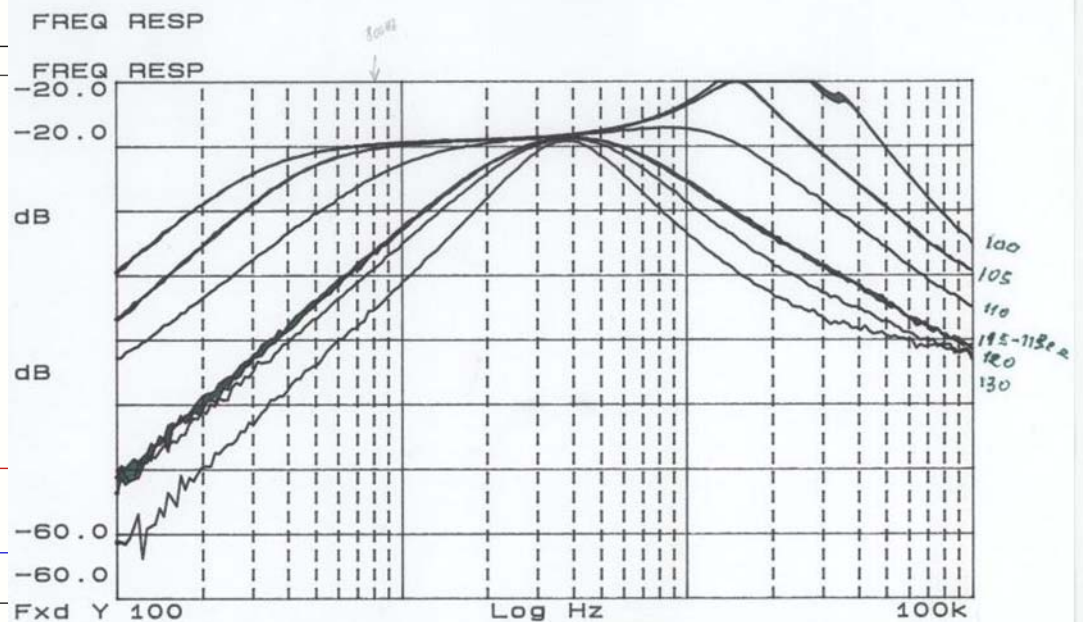
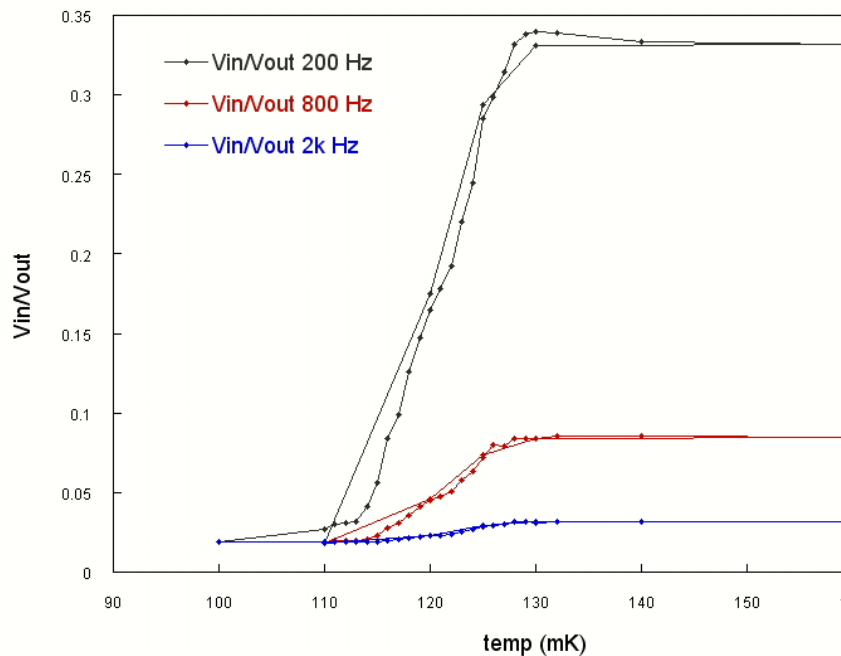
- In a limited region (0.5-5Kz) the current noise equivalent to the input of the transformer is in pA/VHz range.



- The input noise density given by  $R = 1\Omega$  @ 4KHz is measured at different temperatures: it scales as the  $T^{1/2}$ , as expected.



- DC bias will require TES working at a proper R value
- The Transf. Functions along the transition suggests that AC bias should be preferable (see Geleazzi talk)



## Conclusions

- The method of passive cold transformer read-out in trans-resistance configuration is effective (or competitive in term of noise quality) in a limited bandwidth (1 decade: 0.5-5KHz)
- Cold passive electronics, room temperature conventional electronics.
- AC bias configuration should improve the performance, taking the advantage of MUX capability and possibility to extent the bias frequency up to hundreds of MHz.