

**PHY4324–Electromagnetism II**

**Fall 2011**

**Test 2 – 55 minutes**

**Nov. 7, 2011**

*No other materials except calculators allowed. If you can't do one part of a problem, solve subsequent parts in terms of unknown answer—define clearly. Do 2 of 4 problems, CLEARLY indicating which you want graded by circling the problem number!. Each problem is worth 15 pts., for maximum of 30 points.*

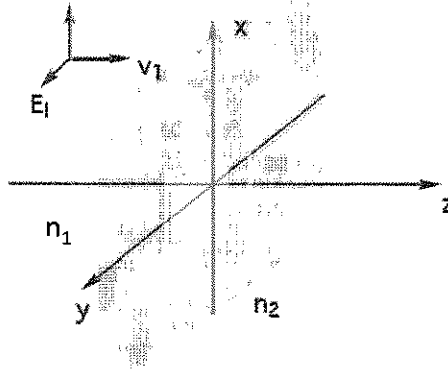


Figure 1: Plane wave in medium 1 traveling along  $z$  incident from left on interface to medium 2.

1. **Plane wave.** Suppose the  $xy$ -plane forms the boundary between two linear media with indices  $n_1$  (take  $\mu = \mu_0$  for both media),  $n_2$ . A plane wave  $\mathbf{E}_I(z, t) = \mathbf{E}_0 e^{ik_1 z - \omega t} \hat{y}$  traveling in the  $z$  direction and polarized in the  $\hat{y}$  direction approaches the interface from the left (figure above).
  - (a) (4 pts.) Calculate  $\mathbf{B}_I(z, t)$  and indicate its direction in the figure.
  - (b) (4 pts.) Write down the form of the reflected electric and magnetic field,  $\mathbf{E}_R(z, t)$ ,  $\mathbf{B}_R(z, t)$  and the transmitted electric and magnetic fields,  $\mathbf{E}_T(z, t)$ ,  $\mathbf{B}_T(z, t)$  respectively.
  - (c) (4 pts.) Write down boundary conditions for the fields at  $z=0$  and use them to calculate the reflected and transmitted  $\mathbf{E}$  fields in terms of incident field, indicating the directions of these fields in the figure.
  - (d) (3 pts.) If medium 2 is a conductor with conductivity  $\sigma$  and permeability  $\mu_0$ , permittivity  $\epsilon$  instead of a dielectric, what is the new form of the transmitted electric field? (For full credit give the mathematical form, the amplitude of the electric field in region 2 in terms of the incident amplitude, and the dispersion relation.)

2. **Parallel-plate waveguide.** A waveguide consists of two infinite parallel plates, as shown. Consider TM waves propagating in the  $+z$  direction, and assume that the fields are *uniform* along the  $x$  direction.

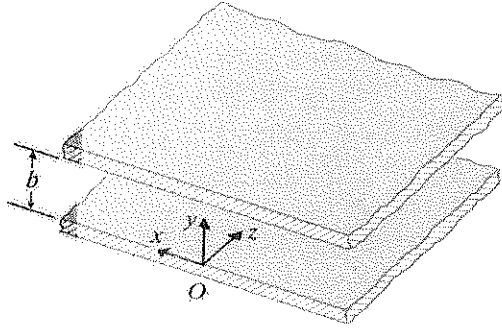


Figure 2: Infinite parallel-plate waveguide

- (a) (4 pts.) State the boundary conditions on the electric and magnetic fields at the inner surfaces of the plates.
- (b) (4 pts.) Write the equation for the  $z$  component of the electric field amplitude  $E_z^0(y)$ , and state the solution, consistent with the boundary conditions you found in (a). (*Hint:* even if you don't know the equation, you should be able to guess the solution.)
- (c) (4 pts.) Using Maxwell's equations, find the transverse components  $B_x^0(y)$  and  $E_y^0(y)$ .
- (d) (3 pts.) Find the dispersion of the TM modes  $\mathbf{k}(\omega)$  and state the cutoff frequency.

3. **Point charge.** The electric field of a moving point charge  $q$  moving at constant velocity  $v\hat{x}$  has the form

$$\mathbf{E}(\mathbf{r}) = \frac{1}{4\pi\epsilon_0} \frac{q}{R^2} \frac{1 - (v/c)^2}{(1 - (v/c)^2 \sin^2 \theta)^{3/2}} \hat{\mathbf{R}}, \quad (1)$$

where  $\theta$  is the angle between the vector  $\mathbf{r}$  and the  $x$  axis, and  $\mathbf{R}$  is the vector from the particle to the field point  $\mathbf{r}$  at the present time.

- (a) (4 pts.) Sketch the electric field lines for the case  $v$  close to  $c$ .
- (b) (4 pts.) Find the magnetic field.
- (c) (4 pts.) Use the result (1) to derive the expression for the electric field of an infinite line charge: assume there are infinitely many charge elements  $dq = \lambda dx$ , each moving with velocity  $v$ , and integrate the charge densities to find the total electric field a distance  $s$  from the axis. *Hint:* You may need  $\int_0^\pi d\theta \sin \theta / (1 - b^2 \sin^2 \theta)$ .
- (d) (3 pts.) Go back to pt. charge moving with velocity  $v$ . At  $t = 0$  the charge is located at the origin  $x = 0$ . How much energy from the point charge is passing through the plane  $\perp$  to the  $x$ -axis at  $x = a$ ? Set up in terms of a  $\theta$ -integral which you need not evaluate. *Hint:* you may need  $\mathbf{A} \times (\mathbf{B} \times \mathbf{C}) = \mathbf{B}(\mathbf{A} \cdot \mathbf{C}) - \mathbf{C}(\mathbf{A} \cdot \mathbf{B})$ .

4. **Wire loop.**

(a) (4 pts.) Using the identities

i.  $\nabla \rho = -\frac{1}{c} \dot{\rho} \hat{z}$  (here  $\rho = \rho(\mathbf{r}', t_r)$ )

ii.  $\nabla \cdot (\hat{z}/z) = 1/z^2$

iii.  $\nabla (1/z) = -\hat{z}/z^2$

iv.  $\nabla \cdot (\hat{z}/z^2) = 4\pi\delta^3(\vec{z})$ ,

and the retarded form of the potential

$$V(\mathbf{r}, t) = \frac{1}{4\pi\epsilon_0} \int d\tau' \frac{\rho(\mathbf{r}', t_r)}{z}, \quad (2)$$

show explicitly that  $\square^2 V = -\frac{1}{\epsilon_0} \rho$ .

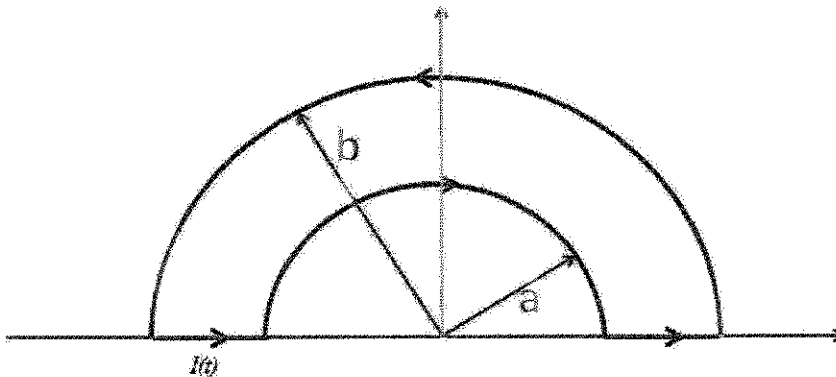


Figure 3: Wire loop with current  $I(t)$  as shown.

The next questions are based on the figure, where a wire is bent into a loop as shown in the figure. Label the two arcs and two segments clearly with numbers 1-4. The goal is to calculate the potentials and fields at  $\vec{r} = 0$  (center of arcs) for a current increasing as  $I = kt$ , where  $k$  is a constant. There is no net charge on the wire.

(b) (4 pts.) Calculate  $\mathbf{A}(\mathbf{r} = 0, t)$  and  $V(\mathbf{r} = 0, t)$ .

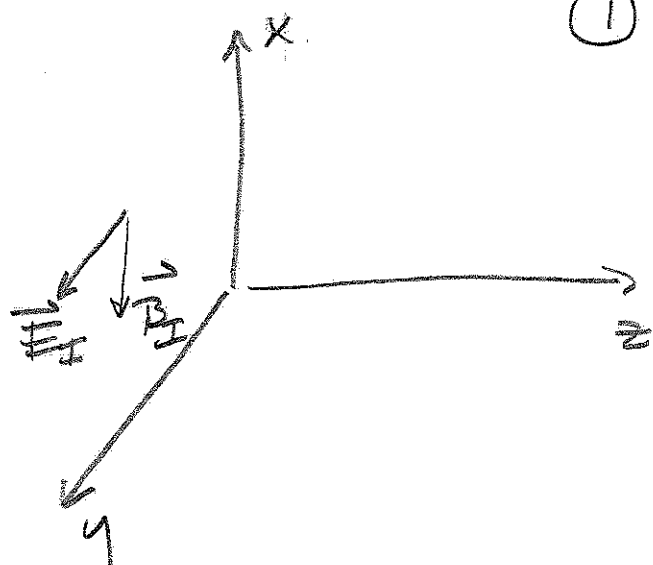
(c) (4 pts.) Calculate  $\mathbf{E}(\mathbf{r} = 0, t)$ .

(d) (3 pts.) Explain how you would go about calculating  $\mathbf{B}(\mathbf{r} = 0, t)$ , but do not do it!

# 1) Plane wave

a) For plane wave in SI units,  $|\vec{B}| = \frac{1}{v} |\vec{E}|$  where  $v$  is velocity of wave in medium.

$\vec{E} \times \vec{B}$  must be in the direction of propagation (Poynting vector), so  $\vec{B}_I \propto -\hat{x}$



$$\Rightarrow \vec{B}_I(z, t) = \frac{E_{0I}}{v_1} e^{i(kz - \omega t)} (-\hat{x})$$

b)  $\vec{E}_R(z, t) = E_{0R} e^{i(-kz - \omega t)}$

$$\vec{B}_R(z, t) = \frac{E_{0R}}{v_1} e^{i(-kz - \omega t)} \hat{x}$$

$$\vec{E}_T(z, t) = E_{0T} e^{i(k_2 z - \omega t)}$$

$$\vec{B}_T(z, t) = \left( \frac{E_{0T}}{v_2} \right) e^{i(k_2 z - \omega t)} (-\hat{x})$$

note  $\vec{B}$  changes sign on reflection!

$$\begin{aligned} v_1 &= \frac{c}{n_1} \\ v_2 &= \frac{c}{n_2} \\ k_1 &= \frac{\omega}{v_1} \\ k_2 &= \frac{\omega}{v_2} \end{aligned}$$

where

$$E_{0R} = \frac{1-\beta}{1+\beta} E_{0I}; \quad E_{0T} = \frac{2}{1+\beta} E_{0I}$$

$$\beta = n_2/n_1 \quad \text{since } \mu_1 = \mu_2 = \mu_0 \text{ given}$$

c) Parallel fields only (normal incidence)

$$\vec{E}_1 \parallel = \vec{E}_2 \parallel; \quad \frac{1}{\mu_1} \vec{B}_1 \parallel = \frac{1}{\mu_2} \vec{B}_2 \parallel$$

$$\Rightarrow \vec{B}_1 \parallel = \vec{B}_2 \parallel$$

Substituting forms from b) gives

$$\frac{E_{0R}}{E_{0I}} \text{ , } \frac{E_{0T}}{E_{0I}} \text{ as in b)}$$

magnitudes of B-ratios same except

$$\frac{B_{0T}}{B_{0I}} = \frac{E_{0T}}{E_{0I}} \cdot \frac{v_1}{v_2}$$

d)  $\vec{E}_T = E_{0T} e^{i(\vec{k}_2 \cdot \vec{r} - \omega t)}$   $\uparrow$

$$\vec{k}_2^2 = \mu_0 \epsilon \omega^2 + i \mu_0 \sigma \omega$$

$$E_{0T} = \frac{2}{1 + \beta} E_{0I}$$

$$\beta = \frac{v_1 \vec{k}_2}{\omega}$$

$\uparrow$   
complex

2) Parallel-plate "waveguide" TM modes (3)

$$E_z = E_z^0 \exp i(kz - \omega t)$$

a) B.C. are

$$E_z^0(y) = 0 \text{ at } y = 0, b$$

$$B_z = 0 \text{ everywhere (TM)}$$

$$b) \left( \frac{\partial^2}{\partial y^2} + \left( \frac{\omega}{c} \right)^2 - k^2 \right) E_z^0 = 0$$

$$\text{soln } E_z^0 = E_0 \sin \frac{n\pi y}{b}$$

$$\Rightarrow \boxed{-\left( \frac{n\pi}{b} \right)^2 + \left( \frac{\omega}{c} \right)^2 = k^2}$$

c) Maxwell  $\Rightarrow$

$$B_x^0 = \frac{i}{\left( \frac{\omega}{c} \right)^2 - k^2} \left( k \frac{\partial B_z}{\partial x} - \frac{\omega}{c} \frac{\partial E_z}{\partial y} \right)$$

$$= \frac{-i E_0}{\left( \frac{\omega}{c} \right)^2 - k^2} \frac{\omega}{c} \left( \frac{n\pi}{b} \right) \cos \frac{n\pi y}{b}$$

$$E_y^0 = \frac{i}{\left( \frac{\omega}{c} \right)^2 - k^2} \left( k \frac{\partial E_z}{\partial y} - \omega \frac{\partial B_z}{\partial x} \right)$$

$$= \frac{i k E_0}{\left( \frac{\omega}{c} \right)^2 - k^2} \left( \frac{n\pi}{b} \right) \cos \frac{n\pi y}{b}$$

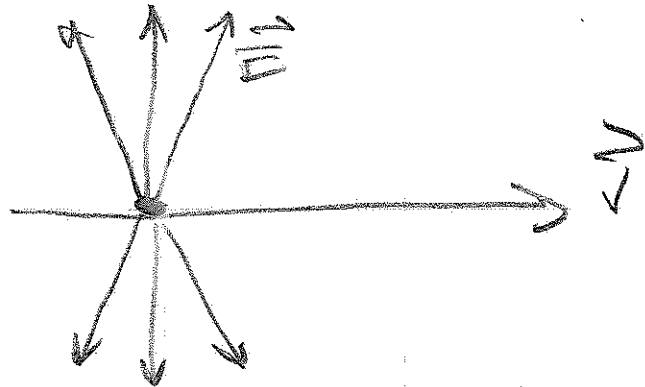
$$d) \text{ From b) } k = \sqrt{\left( \frac{\omega}{c} \right)^2 - \left( \frac{n\pi}{b} \right)^2}$$

$k=0$  gives cutoff  $\boxed{\omega_1 = \frac{c\pi}{b}} \quad n=1 \quad \text{lowest}$



3)  $\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{1 - v/c}{R^2 (1 - (v/c)\sin\theta)^{3/2}} \hat{R}$  (4)

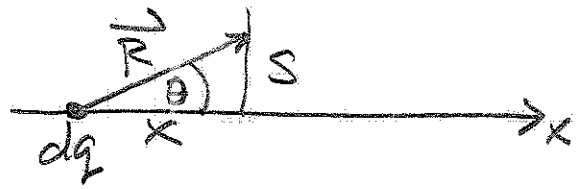
a)



Density of field lines higher  $\perp$  to direction of motion

b)  $\vec{B} = \frac{1}{c^2} \vec{v} \times \vec{E}$

c)  $dq = \lambda dx$



$$\vec{E} = \frac{\lambda}{4\pi\epsilon_0} (1 - v^2/c^2) \int_{-\infty}^{\infty} \frac{d\hat{R}}{R^2} \frac{dx}{(1 - (v/c)\sin\theta)^{3/2}}$$

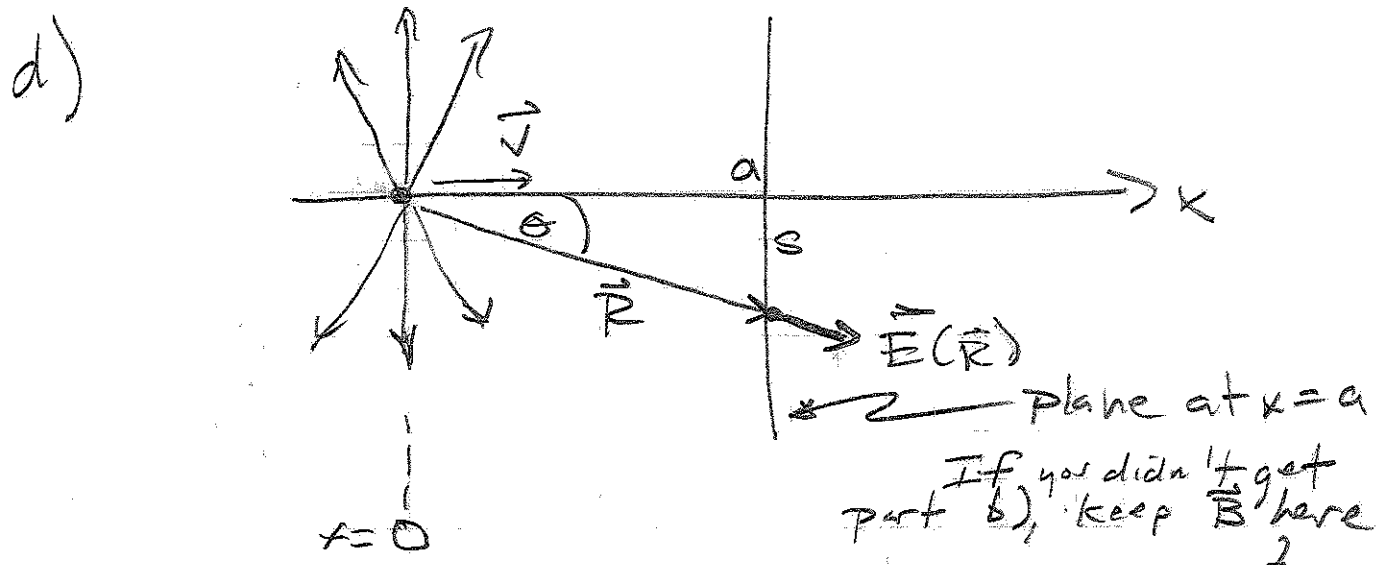
use:  $s = R \sin\theta$ ;  $\frac{1}{R^2} = \frac{\sin^2\theta}{s^2}$

$\frac{x}{s} = \cot\theta$ ;  $dx = s \csc^2\theta d\theta = \frac{s}{\sin^2\theta} d\theta$

$\frac{1}{R^2} dx = \frac{d\theta}{s}$ ;  $(\hat{R})_s = \sin\theta$

$$\Rightarrow \vec{E} = \frac{\lambda}{4\pi\epsilon_0} (1 - (v/c)^2) \left(\frac{1}{s}\right) \int_0^\pi d\theta \frac{\sin\theta}{(1 - (v/c)\sin\theta)^{3/2}} \cdot \frac{1}{2 \cdot (1 - v/c)^2}^{-1}$$

$= \frac{\lambda}{2\pi\epsilon_0 s} \hat{s}$  as for line chg. at rest.



$\vec{S} = \frac{1}{\mu_0} (\vec{E} \times \vec{B}) = \frac{1}{\mu_0 c^2} \vec{E} \times (\vec{v} \times \vec{E})$

BAC-CAB!  $\Rightarrow = \epsilon_0 (\vec{v} E^2 - \vec{E} (\vec{v} \cdot \vec{E}))$

Power thru plane  $= \int_{\text{plane}} \vec{S} \cdot d\vec{a} = \epsilon_0 \int (v E^2 - \frac{v}{x} E^2) 2\pi s ds$

$d\vec{a} = 2\pi s ds \hat{x}$

$E_x = E \cos \theta$   
 $E^2 - E_x^2 = E^2 \sin^2 \theta$

$P = 2\pi v \epsilon_0 \int E^2 \cdot (a \tan \theta) \left( \frac{a d\theta}{\cos^2 \theta} \right) \sin^2 \theta$

$E = \frac{q}{4\pi\epsilon_0 R^2} \frac{1-\beta^2}{(1-\beta^2 \sin^2 \theta)^{3/2}}$

$s = a \tan \theta$   
 $ds = \frac{a d\theta}{\cos^2 \theta}$

so  $P = \frac{2\pi v q^2}{(4\pi)^2 \epsilon_0} \frac{(1-\beta^2)^2}{a^2} \int_0^\pi d\theta \frac{\sin^3 \theta \cos \theta}{(1-\beta^2 \sin^2 \theta)^{3/2}}$

Full credit

$= \frac{q^2 v}{2\pi \epsilon_0 a^2}$

# 4) Wire loop

(6)

(a) Show  $\square^2 V = -\frac{1}{\epsilon_0} \rho$

$$\square^2 = \nabla^2 - \frac{1}{c^2} \frac{\partial^2}{\partial t^2}$$

Start with

$$\nabla V = \frac{1}{4\pi\epsilon_0} \int dz' \left( \frac{\nabla \rho(\vec{r}', t_r)}{r} + \rho(\vec{r}', t_r) \vec{\nabla} \frac{1}{r} \right)$$

$$= \frac{1}{4\pi\epsilon_0} \int dz' \left( \underbrace{\frac{-c\dot{\rho}\hat{r}}{r}}_{\text{i}} + \rho \underbrace{\left( \frac{-\hat{r}}{r^2} \right)}_{\text{iii}} \right)$$

$$\begin{aligned} \text{So } \nabla \cdot \nabla V &= \frac{1}{4\pi\epsilon_0} \int dz' \left[ -\frac{1}{c} \frac{(c\dot{\rho})\hat{r}}{r} - \frac{1}{c} \dot{\rho} \vec{\nabla} \left( \frac{\hat{r}}{r^2} \right) \right. \\ &\quad \left. + \vec{\nabla} \rho \left( \frac{\hat{r}}{r^2} \right) - \rho \nabla \left( \frac{\hat{r}}{r^2} \right) \right] \end{aligned}$$

$$= \frac{1}{4\pi\epsilon_0} \int dz' \left[ \frac{1}{c^2} \ddot{\rho} \frac{\hat{r}}{r} - \frac{1}{c} \dot{\rho} \frac{\hat{r}}{r^2} + \frac{1}{c} \dot{\rho} \frac{\hat{r}}{r^2} - \rho 4\pi \delta^{(3)} \left( \frac{\vec{r}}{r} \right) \right] \quad \text{iv}$$

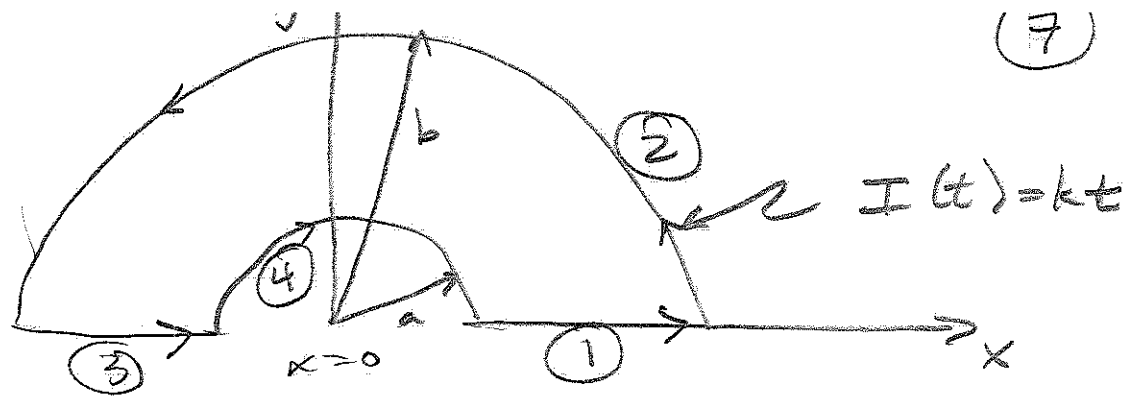
$$= \frac{1}{4\pi\epsilon_0} \int dz' \left( -\frac{1}{c^2} \ddot{\rho} \frac{\hat{r}}{r} \right) - \frac{1}{\epsilon_0} \rho(\vec{r}, t)$$

Also:  $\frac{\partial^2}{\partial t^2} V = \frac{1}{4\pi\epsilon_0} \int dz' \frac{\ddot{\rho}(\vec{r}', t_r)}{r}$

$\delta$ -Fct sets  $\vec{r} = \vec{r}'$

since  $\frac{\partial}{\partial t} t_r = \frac{\partial}{\partial t} (t - r/c) = 1$

$$\text{So } \square^2 V = \left( \nabla^2 - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \right) V = -\frac{1}{\epsilon_0} \rho(\vec{r}, t) \quad \checkmark$$



$$\begin{aligned}
 (b) \quad \vec{A}(\vec{r}=0, t) &= \frac{\mu_0}{4\pi} \oint \frac{I(t_r)}{r} dl' \\
 &= \frac{\mu_0}{4\pi} k \oint \left( \frac{t - r/c}{r} \right) dl' \\
 &= \frac{\mu_0 k}{4\pi} t \oint \frac{dl'}{r} \quad \text{since 2nd term} \\
 &\quad \propto \oint dl' = 0!
 \end{aligned}$$

So we need  $\mu$  on ①...④

Since  $\vec{r}=0$ ,  $\mu = r'$

$$\textcircled{1} \quad r' = x' \quad \textcircled{2} \quad r' = b \quad \textcircled{3} \quad r' = -x' \quad \textcircled{4} \quad r' = a$$

$$\Rightarrow \oint \frac{dl'}{\mu} = \int_a^b \frac{dx'}{x'} + \int_0^\pi \frac{b d\theta}{b} + \int_{-b}^{-a} \left( \frac{dx'}{-x'} \right) + \int_\pi^0 \frac{a d\theta}{a}$$

← cancel →

$$= \textcircled{1} + \textcircled{3} = 2 \int_a^b \frac{dx'}{x'} = 2 \ln \frac{b}{a} \hat{x}$$

$$\Rightarrow \vec{A}(\vec{r}=0, t) = \frac{\mu_0 k t}{2\pi} \ln \frac{b}{a} \hat{x}$$

and  $V(\vec{r}=0, t) = 0$  since  $\rho = 0$

$$c) \vec{E}(\vec{r}=0, t) = -\nabla V + \frac{\partial \vec{A}}{\partial t}$$

$$= 0 + \frac{\mu_0 k}{2\pi} \ln \frac{b}{a} \hat{x}$$

induced by  
+ - changing  
 $\vec{B}$ -field!

d) Can't calculate  $\vec{B}$

from  $\nabla \times \vec{A}$  unless we know  $\vec{A}$   
in a neighborhood of  $\vec{r}=0$ . So  
far we have  $\vec{A}$  only at one point!

So go back & calculate  $\vec{A}$  for some  
neighborhood, take curl OR use Jefimenko:

$$\vec{B}(\vec{r}=0, t) = \frac{\mu_0}{4\pi} \int \left[ \frac{\vec{I}(\vec{r}', t_r)}{r'^2} + \frac{\dot{\vec{I}}(\vec{r}', t_r)}{c r'} \right] d\vec{l}' \times \hat{r}'$$