

PHY3113–Introduction to Theoretical Physics

Fall 2007

Test 2 SOLUTIONS

Oct. 26, 2007

Useful formulae:

$$\vec{\nabla}\psi = \frac{\partial\psi}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial\psi}{\partial\theta} \hat{\theta} + \frac{1}{r \sin\theta} \frac{\partial\psi}{\partial\phi} \hat{\phi}.$$

$$\vec{\nabla} \cdot \vec{A} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 A_r) + \frac{1}{r \sin\theta} \frac{\partial}{\partial\theta} (\sin\theta A_\theta) + \frac{1}{r \sin\theta} \frac{\partial A_\phi}{\partial\phi}$$

$$x = r \sin\theta \cos\phi = \rho \cos\vartheta$$

$$y = r \sin\theta \sin\phi = \rho \sin\vartheta$$

$$z = r \cos\theta = z$$

$$\nabla \cdot \vec{E} = \rho/\epsilon_0$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{E} = -\frac{\partial\vec{B}}{\partial t}$$

$$\nabla \times \vec{B} = \mu_0 \vec{j} + \mu_0 \epsilon_0 \frac{\partial\vec{E}}{\partial t}$$

$$\vec{E} = -\nabla\Phi$$

$$\vec{B} = \nabla \times \vec{A}$$

$$\vec{\nabla}\psi = \sum_i \hat{q}_i \frac{1}{h_i} \frac{\partial\psi}{\partial q_i}.$$

1. For each matrix  $A$ , calculate  $A^\dagger$ ,  $\det A$  and  $A^{-1}$ . On this basis, state whether each is Hermitian, unitary, and/or orthogonal, ...:

(a)

$$A^\dagger = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}, \det A = -1, C^T = \begin{bmatrix} 0 & -1 \\ -1 & 0 \end{bmatrix}, A^{-1} = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} \quad (1)$$

$$A^{-1} = A^\dagger, \text{unitary or orthogonal}, \quad (2)$$

$$A = A^\dagger, \text{hermitian}. \quad (3)$$

(b)

$$A^\dagger = \begin{bmatrix} 2 & 1+i \\ 1-i & 3 \end{bmatrix}, \det A = 6 - 2 = 4, \quad (4)$$

$$C = \begin{bmatrix} 3 & -(1-i) \\ -(1+i) & 2 \end{bmatrix}, C^T = \begin{bmatrix} 3 & -(1+i) \\ -(1-i) & 2 \end{bmatrix}, \quad (5)$$

$$A^{-1} = \frac{1}{4} \begin{bmatrix} 3 & -(1+i) \\ -(1-i) & 2 \end{bmatrix} = \begin{bmatrix} 3/4 & (-1-i)/4 \\ -(1-i)/4 & 1/2 \end{bmatrix}. \quad (6)$$

since  $A = A^\dagger$ , hermitian

(c)

$$A^{-1} = \begin{bmatrix} \cos \alpha & 0 & \sin \alpha \\ 0 & 1 & 0 \\ -\sin \alpha & 0 & \cos \alpha \end{bmatrix}, A^{-1} = A^\dagger \quad (7)$$

*orthogonal* or *unitary* (real). Note this is a rotation about the  $y$  axis by angle  $\alpha$ , so inverse is just rotation by  $-\alpha$ .

(d) Solve the system of equations

$$\begin{bmatrix} 8 & -2/3 \\ -4 & 1/2 \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \quad (8)$$

explicitly by Cramer's rule.

$$\det \begin{bmatrix} 8 & -2/3 \\ -4 & 1/2 \end{bmatrix} = \frac{4}{3} \quad (9)$$

so

$$x = \frac{3}{4} \det \begin{bmatrix} 1 & -2/3 \\ 1 & 1/2 \end{bmatrix} = \frac{7}{8}$$
$$y = \frac{3}{4} \det \begin{bmatrix} 8 & 1 \\ -4 & 1 \end{bmatrix} = 9$$

2. Evaluate

(a)

$$\int_{-\infty}^{\infty} dx \delta(2x - \pi) \sin x = \frac{1}{2} \int_{-\infty}^{\infty} dx \delta(x - \frac{\pi}{2}) \sin x = \frac{1}{2}. \quad (10)$$

(b)

$$\int_{\pi/4}^{3\pi/4} d\theta \delta(\cos \theta)(\sin^2 \theta + 1) = \int_{\pi/4}^{3\pi/4} dx \frac{\delta(\theta - \frac{\pi}{2})}{|\sin \theta|_{\theta=\pi/2}} (\sin^2 \theta + 1) = 2. \quad (11)$$

(c)

$$\int d\tau \delta(r - a) = \int_0^\infty r^2 \delta(r - a) dr \int_0^\pi \sin \theta d\theta \int_0^{2\pi} d\phi = 4\pi a^2. \quad (12)$$

(d) What is the charge density  $\rho(x, y, z)$  for an infinitely long but infinitesimally thick line of charge, with charge per unit length  $\lambda$ , oriented parallel to the  $x$  axis passing through the point  $(0,1,0)$ ?

We know it must be proportional to  $\delta(y-1)\delta(z)$ , and that when we integrate over  $y$  and  $z$  in a plane perpendicular to the wire, we should recover the full charge density per unit length along  $x$ . Thus A

$$\int dy \int dz \delta(y - 1)\delta(z) = \lambda, \quad (13)$$

so that

$$\rho = \lambda \delta(y - 1)\delta(z). \quad (14)$$

Note this has dimensions of charge/ 3D volume.

3. Given a vector field  $\vec{F} = r \cos \theta \hat{r} + 2r\hat{\theta} + 2r \cos \theta \sin \phi \hat{\phi}$ , calculate

(a)

$$\begin{aligned} \vec{\nabla} \cdot \vec{F} &= \frac{1}{r^2} \frac{\partial}{\partial r} (r^3 \cos \theta) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (2r \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial (2r \cos \theta \sin \phi)}{\partial \phi} \\ &= 3 \cos \theta + 2 \cot \theta + 2 \cot \theta \cos \phi. \end{aligned} \quad (15)$$
$$(16)$$

(b) (volume is sphere radius 1)

$$\begin{aligned} \int_{\tau} \vec{\nabla} \cdot \vec{F} d\tau &= \int_0^1 r^2 dr \int_0^\pi \sin \theta d\theta \int_0^{2\pi} d\phi (3 \cos \theta + 2 \cot \theta + 2 \cot \theta \cos \phi) \\ &= \frac{1}{3} \times 0 = 0. \end{aligned} \quad (17)$$

(c) (area is surface of sphere radius 1)

$$d\vec{a} = \sin \theta d\theta d\phi \hat{r}, \quad (18)$$

$$\vec{F} \cdot d\vec{a} = \sin \theta \cos \theta d\theta d\phi. \quad (19)$$

$$\int_A \vec{F} \cdot d\vec{a} = 2\pi \frac{1}{2} \sin^2 \theta \Big|_0^\pi = 0. \quad (20)$$

(d) So Gauss's theorem is satisfied by comparing b) and c).

4. (a)-(b) First notice that since  $\vec{A}$  points along  $\hat{y}$  and is  $\propto x$ , the only contribution to line integral is along segment parallel to  $y$  axis at  $x = a$ .  $\vec{A}$  is const. along this segment, so integral is trivial. The curl of  $\vec{A}$  which we need for Stokes' thm. is just the magnetic field  $\vec{B}$ , and taking the curl leads to a constant  $\vec{B}$  field pointing along  $z$ , which is constant over the top face of the cube. Its dot product with the normals of all other faces is zero, so

$$\oint \vec{A} \cdot d\vec{r} = \int_0^a B_0 a dy = B_0 a^2. \quad (21)$$

$$\vec{B} = B_0 \hat{k}, \quad (22)$$

$$\int B \cdot d\vec{a} = B_0 a^2 = \oint \vec{A} \cdot d\vec{r}. \quad (23)$$

Now suppose the magnetic field is increasing with time,  $B_0(t) = \alpha t$ , and that the cube is an open framework of wires on its edges. Each wire segment has resistance  $R$ .

- (c) What is  $\nabla \times \vec{E}$  generated in the space around the cube?

Here we need to use Faraday's eqn.  $\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$ . The term on the right hand side of Faraday's law is  $-\alpha$ , so  $\vec{\nabla} \times \vec{E} = -\alpha \hat{k}$ .

- (d) The line integral of this electric field around the square in the  $xy$  plane,  $\oint_{\square} \vec{E} \cdot d\vec{\ell}$ , is the induced voltage, or EMF. What current flows in the wire square?

$$\oint \vec{E} \cdot d\vec{\ell} = \int \vec{\nabla} \times \vec{E} \cdot d\vec{a} = -\alpha a^2. \quad (24)$$

Ohm's law says  $I = V/R = -\alpha a^2/(4R)$  (since segment resistances add in series), so  $I = -\alpha a^2/(4R)$ .

5. (a)-(b) Calculate the arc length  $ds^2$  and scale factors  $h_i$  for the cylindrical coordinate system  $\rho, \vartheta, z$ .

$$x = r \cos \vartheta, \quad y = r \sin \vartheta, \quad z = z, \quad (25)$$

$$dx = \frac{\partial x}{\partial r} dr + \frac{\partial x}{\partial \vartheta} d\vartheta + \frac{\partial x}{\partial z} dz = \cos \vartheta dr - r \sin \vartheta d\vartheta, \quad (26)$$

$$dy = \sin \vartheta dr + r \cos \vartheta d\vartheta, \quad (27)$$

$$dz = dz, \quad (28)$$

$$ds^2 = dx^2 + dy^2 + dz^2 = dr^2 + r^2 d\vartheta^2 + dz^2. \quad (29)$$

$$h_r = 1, \quad h_\vartheta = r, \quad h_z = 1, \quad (30)$$

$$\vec{\nabla} \psi = \sum \hat{q}_i \frac{1}{h_i} \frac{\partial \psi}{\partial q_i} = \hat{r} \frac{\partial \psi}{\partial r} + \frac{\hat{\vartheta}}{r} \frac{\partial \psi}{\partial \vartheta} + \hat{z} \frac{\partial \psi}{\partial z}. \quad (31)$$

- (c) Write down an expression in terms of the unit vectors  $\hat{\rho}$ ,  $\hat{\vartheta}$ , and  $\hat{z}$ , for the unit vector normal to the surface of a cone of height  $h$  and base radius  $r$ .

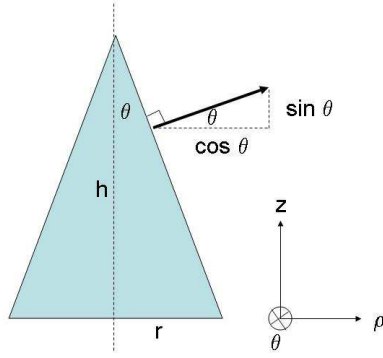


FIG. 1: cross section of cone.

Components of normal unit vector are shown,  $\vartheta = \tan^{-1} r/h$ , so  $\hat{n} = \cos \vartheta \hat{\rho} + \sin \vartheta \hat{z}$ .

(d) Find expressions for  $\hat{\rho}$ ,  $\hat{\vartheta}$ , and  $\hat{z}$  in terms of  $\hat{i}$ ,  $\hat{j}$ , and  $\hat{k}$ .

$$d\vec{s} = dx\hat{i} + dy\hat{j} + dz\hat{k} \quad (32)$$

$$= d\rho\hat{\rho} + \rho d\vartheta\hat{\vartheta} + dz\hat{z} \quad (33)$$

Now we calculate  $dx = \frac{\partial x}{\partial \rho} d\rho + \frac{\partial x}{\partial \vartheta} d\vartheta + \frac{\partial x}{\partial z} dz$ , etc., and equate coefficients of  $d\rho$ , etc. to find

$$\begin{aligned} \hat{\rho} &= \hat{i} \cos \vartheta + \hat{j} \sin \vartheta \\ \hat{\vartheta} &= -\hat{i} \sin \vartheta + \hat{j} \cos \vartheta \\ \hat{z} &= \hat{k} \end{aligned} \quad (34)$$

6. A vector field has the form

$$\vec{A}(x, y, z) = (x + \alpha y, y + \beta x, z) \quad (35)$$

(a) Determine  $\alpha$  and  $\beta$  such that  $\nabla \times \vec{A} = 0$ .

$$\begin{aligned} \vec{\nabla} \times \vec{A} &= \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \partial_x & \partial_y & \partial_z \\ x + \alpha y & y + \beta x & z \end{vmatrix} \\ &= \hat{k}(\beta - \alpha) = 0, \end{aligned}$$

so  $\alpha = \beta$  works  $\forall \alpha$ .

- (b) Calculate the corresponding scalar potential  $\Phi$ . Be sure to clearly specify all unknown constants.

Using definition  $\vec{A} = -\vec{\nabla}\Phi$ , we have

$$\begin{aligned}\partial_x \Phi &= -x - \alpha y \\ \partial_y \Phi &= -y - \alpha x \\ \partial_z \Phi &= -z\end{aligned}$$

First condition  $\Rightarrow \Phi = -x^2/2 - xy\alpha + c(y, z)$ , second one  $\Rightarrow \partial_y c(y, z) = -y \Rightarrow c(y, z) = -y^2/2 + c(z)$ , third one  $\Rightarrow \partial_z c(z) = -z \Rightarrow c(z) = -z^2/2 + c$ . So

$$\Phi = -\frac{1}{2}(x^2 + y^2 + z^2) - \alpha xy + c \quad (36)$$

- (c) Sketch the vector field  $\vec{A}$  in the plane  $z = 0$  for  $\alpha = 1$ .

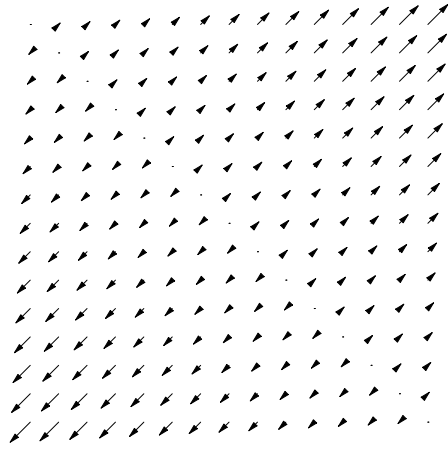


FIG. 2: Plot with  $\alpha = 1$  with  $x, y$  running from -1 to 1.

- (d) Calculate the ratio of the line integrals

$$\frac{\int_{s_1} \vec{A} \cdot d\vec{r}}{\int_{s_2} \vec{A} \cdot d\vec{r}}, \quad (37)$$

where  $s_1$  is the path along the diagonal between  $a = (0, 0, 0)$  and  $b = (1, 1, 1)$ , and  $s_2$  is the path  $a \rightarrow (1, 0, 0) \rightarrow (1, 1, 0) \rightarrow b$ .

Without doing any calculations, we know the ratio is 1, since the field is conservative ( $\nabla \times \vec{v} = 0$ ), so the line integral is independent of the path taken.